K & I

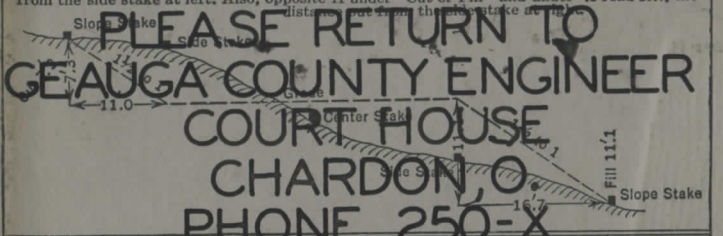
FIELD BOOK

I 360

DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING

Roadway of any Width. Side Slopes 1½ to 1.

In the figure below: opposite 7 under "Cut or Fill" and under .3 read 11.0, the distance out from the side stake at left. Also, opposite 11 under "Cut or Fill" and under .1 read 16.7, the distance out from the side stake at right.



Cut or Fill	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	Cut or Fill
	Distance out from Side or Shoulder Stake										
0	0.0	0.2	0.3	0.5	0.6	0.8	0.9	1.1	1.2	1.4	0
1	1.5	1.7	1.8	2.0	2.1	2.3	2.4	2.6	2.7	2.9	1
2	3.0	3.2	3.3	3.5	3.6	3.8	3.9	4.1	4.2	4.4	2
3	4.5	4.7	4.8	5.0	5.1	5.3	5.4	5.6	5.7	5.9	3
4	6.0	6.2	6.3	6.5	6.6	6.8	6.9	7.1	7.2	7.4	4
5	7.5	7.7	7.8	8.0	8.1	8.3	8.4	8.6	8.7	8.9	5
6	9.0	9.2	9.3	9.5	9.6	9.8	9.9	10.1	10.2	10.4	6
7	10.5	10.7	10.8	11.0	11.1	11.3	11.4	11.6	11.7	11.9	7
8	12.0	12.2	12.3	12.5	12.6	12.8	12.9	13.1	13.2	13.4	8
9	13.5	13.7	13.8	14.0	14.1	14.3	14.4	14.6	14.7	14.9	9
10	15.0	15.2	15.3	15.5	15.6	15.8	15.9	16.1	16.2	16.4	10
11	16.5	16.7	16.8	17.0	17.1	17.3	17.4	17.6	17.7	17.9	11
12	18.0	18.2	18.3	18.5	18.6	18.8	18.9	19.1	19.2	19.4	12
13	19.5	19.7	19.8	20.0	20.1	20.3	20.4	20.6	20.7	20.9	13
14	21.0	21.2	21.3	21.5	21.6	21.8	21.9	22.1	22.2	22.4	14
15	22.5	22.7	22.8	23.0	23.1	23.3	23.4	23.6	23.7	23.9	15
16	24.0	24.2	24.3	24.5	24.6	24.8	24.9	25.1	25.2	25.4	16
17	25.5	25.7	25.8	26.0	26.1	26.3	26.4	26.6	26.7	26.9	17
18	27.0	27.2	27.3	27.5	27.6	27.8	27.9	28.1	28.2	28.4	18
19	28.5	28.7	28.8	29.0	29.1	29.3	29.4	29.6	29.7	29.9	19
20	30.0	30.2	30.3	30.5	30.6	30.8	30.9	31.1	31.2	31.4	20
21	31.5	31.7	31.8	32.0	32.1	32.3	32.4	32.6	32.7	32.9	21
22	33.0	33.2	33.3	33.5	33.6	33.8	33.9	34.1	34.2	34.4	22
23	34.5	34.7	34.8	35.0	35.1	35.3	35.4	35.6	35.7	35.9	23
24	36.0	36.2	36.3	36.5	36.6	36.8	36.9	37.1	37.2	37.4	24
25	37.5	37.7	37.8	38.0	38.1	38.3	38.4	38.6	38.7	38.9	25
26	39.0	39.2	39.3	39.5	39.6	39.8	39.9	40.1	40.2	40.4	26
27	40.5	40.7	40.8	41.0	41.1	41.3	41.4	41.6	41.7	41.9	27
28	42.0	42.2	42.3	42.5	42.6	42.8	42.9	43.1	43.2	43.4	28
29	43.5	43.7	43.8	44.0	44.1	44.3	44.4	44.6	44.7	44.9	29
30	45.0	45.2	45.3	45.5	45.6	45.8	45.9	46.1	46.2	46.4	30
31	46.5	46.7	46.8	47.0	47.1	47.3	47.4	47.6	47.7	47.9	31
32	48.0	48.2	48.3	48.5	48.6	48.8	48.9	49.1	49.2	49.4	32
33	49.5	49.7	49.8	50.0	50.1	50.3	50.4	50.6	50.7	50.9	33
34	51.0	51.2	51.3	51.5	51.6	51.8	51.9	52.1	52.2	52.4	34
35	52.5	52.7	52.8	53.0	53.1	53.3	53.4	53.6	53.7	53.9	35
36	54.0	54.2	54.3	54.5	54.6	54.8	54.9	55.1	55.2	55.4	36
37	55.5	55.7	55.8	56.0	56.1	56.3	56.4	56.6	56.7	56.9	37
38	57.0	57.2	57.3	57.5	57.6	57.8	57.9	58.1	58.2	58.4	38
39	58.5	58.7	58.8	59.0	59.1	59.3	59.4	59.6	59.7	59.9	39
40	60.0	60.2	60.3	60.5	60.6	60.8	60.9	61.1	61.2	61.4	40

KEUFFEL & ESSER CO., N. Y.

For Curve Tables see end of book.

Return To
COUNTY ENGINEER
Chardon, Ohio

The paper in this book No. F360
is made of 100% high grade rag stock
with a WATER RESISTING surface sizing.

Book 166

INDEX

9-12-41 Pomeroy
9-13-41 Randles C.H.12

FULLERTOWN ROAD

Construction

Grades at 1st Curve

Stakes set 15' off ℄

B.M.	6.51	1087.87		1081.36	Grade
T.P.	9.15	1094.78	2.24	1085.63	of E. berm
118+50					1085.0
119+0					1086.15
+50					1086.70
120+0					1087.33
T.P.	10.29	1096.07	7.00	1085.78	
+50					1088.66
121+0					1090.02
+50					1091.26
T.P.	7.12	1099.64	3.55	1092.52	
B.M. (Set)	0.23	1099.64	0.23	1099.41	
T.P.	0.63	1092.39	7.88	1091.76	
T.P.	3.42	1087.20	8.61	1083.78	
B.M.			5.85	1081.35	(1081.36)

SEC. S D E F

Stake		Rod	Rod	Grd	Stake	
9.38	G	9.38	9.78	9.8	9.28	C 0'-6"
8.34	F 1'-0"	7.34	8.63	8.65	7.65	C 1'-0"
8.56	F 2'-6"	6.06	8.08	8.40	7.58	C 0'-6"
8.50	F 3'-6"	5.00	7.45	7.60	6.95	C 0'-6"
9.61	F 4'-0"	5.61	7.41	8.0	7.41	G
5.50	F 0'-6"	5.00	6.05	6.76	5.30	C 0'-9"
4.24	C 0'-6"	4.74	4.81	5.38	3.06	C 1'-9"

Spk SW root Pine 123± 20 Rt 29'

Sections for proposed new
Taken 90° to tangent stations except

BM 13	11.58	1117.68	1106.10
182+00			
+50			
183+00			
	4.89	1110.99	1106.10
+50			
184+00			
+50			
185+00			

Curve at Cedar Rd

183+50 bisecting angle

Drill hole 24" from E end Conc. Hdwl.

4.8/E 5.0/8 5.6/12 4.8/15 4.6/22 2.1/25 2.0/34 LF →

7.9/E 8.3/11 8.7/13 8.3/17 7.7/19.5 3.5/29 4.3/40

10.4/E 10.0/5 11.4/18 10.6/33 8.3/26 8.0/35 8.5/50 9.1/56

4.4/E 4.5/18.5 6.0/33.5 6.9/44 7.3/62 7.0/72

5.3/E 5.2/5 6.8/20 8.4/27 9.0/40 9.1/60

5.9/E 6.3/8.5 7.3/16.5 9.3/44

6.0/E 6.4/12 6.9/15 7.5/16 6.9/19 6.4/34

open field on Worthington
brush & small trees on Mansfield

183+02		53'	8 W.Ch.
+80		31'	14" Apple
+45		31'	14" Apple
182+08		31'	14" Apple

Grades at 2nd Curve
Stakes set 16' off ℄

B.M.	10.15	1078.98		1068.83
139+0				
+50				
138+0				
T.P.	7.19	1085.10	1.07	1077.91
+50				
137+0				
+50				
136+0				

Note: Grades as given on plans not used.

Lt Stk	Lt Gd	Lt Rod	Rt Rod	Rt Gd	Rt Stk
5.53 C1'-3"	5.64	5.78	5.30	6.05	4.55 C0'-9"
3.55 C0'-9"	4.05	4.28	2.96	4.14	2.23 C0'-9"
1.06 C1'-3"	2.16	2.31	0.36	1.66	0.11 C0'-3"
4.06 C2'-0"	5.30	6.10	3.81	5.04	3.78 G
3.76 C1'-6"	4.38	5.26	3.25	3.86	2.25 C1'-0"
4.17 C2'-3"	5.55	6.42	5.04	4.50	2.54 C2'-6"
6.00 C0'-6"	6.96	6.53	5.96	7.0	7.93 F2'-0"

4-7-42 Pomeroy Gundersen Hosford

LEVELS VOYTKO

	+	HI	−	E
72+0				1181.4
T.P.	3.01	1190.52		1187.51
300 W				1179.4
200 W				1179.2
T.P.	6.61	1192.70		1186.09
T.P.	rain 11:30		7.53	1186.09
100' W				1179.9
W. F.L.				1180.4
T.P.			6.11	1187.51
73+0				1180.3
74+0				1180.7
74+90				1179.9
B.M.			7.37	1186.25
T.P.	1.98	1193.62	12.25	1191.64
T.P.	0.08	1203.89	12.36	1203.81
T.P.	0.18	1216.17	12.64	1215.99
T.P.	1.03	1228.63	6.79	1227.60
B.M.	2.36	1234.39		1232.03

DITCH

S (Lft) ℄ N (rt)

3.51 4.8 7.4 9.1 7.4
S+K 15 5 15

13.3

13.5

Large rock

13.7

13.2

S+K 73

6.11
S+K

13.3

7.67 9.0 12.2 12.7 12.3 11.1
S+K 15 6 6 15

8.13
S+K

13.7
F.L.

Spike N.W. root 22" Elm ± 25' S.E of S end bridge

X S.E. 4 of Conc. Hdwl N.E quadrant of intersection Chardon-Auburn road & Chag. Falls - Greenville road.

	+	HI	—	E
F.L. (S)				1193.6
B.M.	1.77	1204.87		1203.10
61				
T.P.			4.79	1185.21
62				1182.6
63				1182.4
64				(82.8) 1185.0
65				1183.0
B.M.			2.04	1187.96
66				1182.2
67				1181.2
T.P.	3.07	1190.00	3.59	1186.93
68				1180.6
69				1181.3
70				1181.0
71				1181.4
		1190.52		

S E N 6

11.3

B.M. #3 Stafford road. Spk S. root 28" Maple 25' Lt. Sta. 17+10

Stopped for high H_2O S+K rock (see page 11)

5.2 25 — 7.4 — 5.2 50

7.6 — 4.16 S+K

5.7 24 — 7.2 15 — 5.7 4 — 5.0 — 3.8 12 — 3.24 S+K

7.0 — 6.1 15 — 4.67 S+K

Top large boulder 66 to 40' Rt

6.8 15 — 7.8 — 5.8 6 — 3.7 15 — 2.26 S+K

8.8 — 2.57 S+K

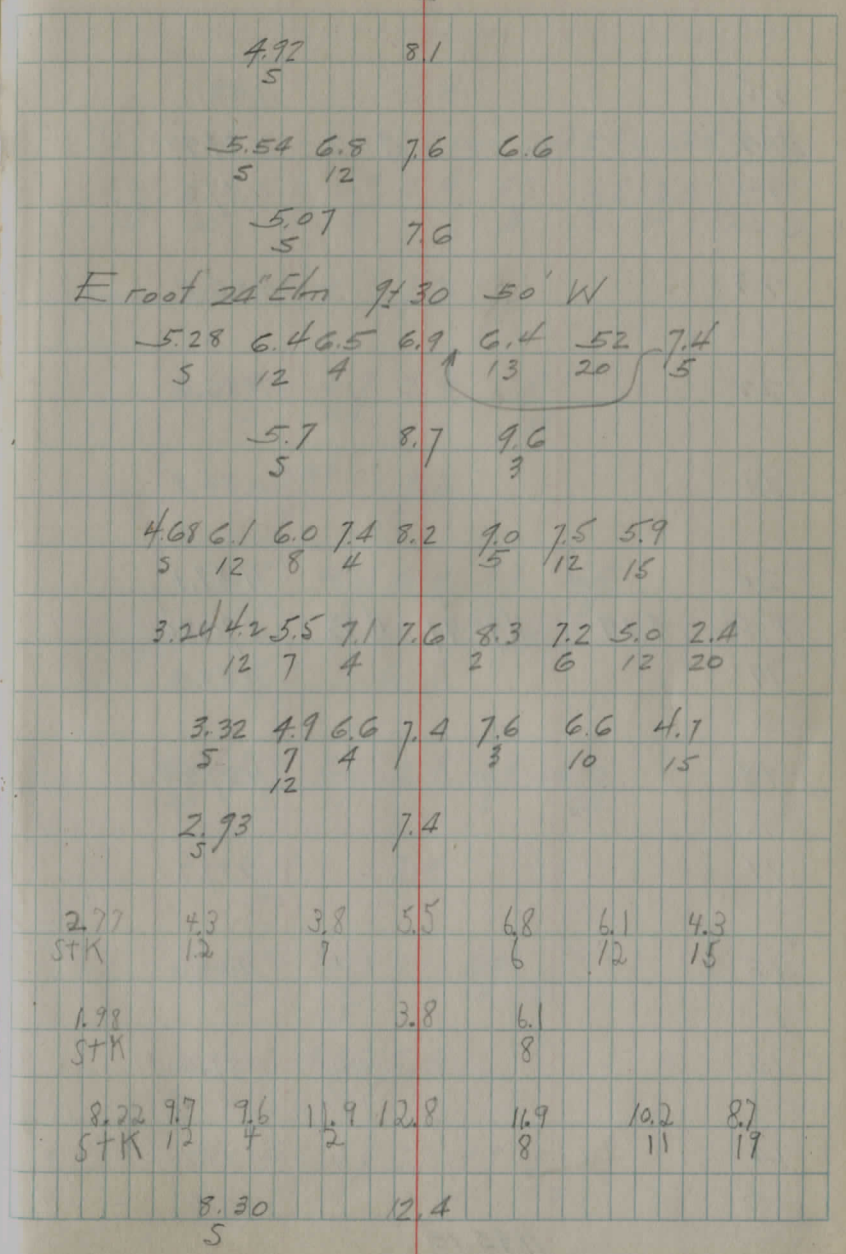
6.7 15 — 9.9 — 6.7 15 — 5.50 S+K

9.2 — 2.63 S+K

S+K 5.9 15 — 7.1 6 — 9.5

3.68 S+K — 9.1

	+	H.I.	−	E
T.P.	4.92	1195.13	5.97	1190.21
13				1188.1
12				1188.6
10+95				1188.6
B.M.			3.92	1192.26
10				1189.3
T.P.	3.99	1196.18	5.68	1192.19
9				1189.2
8				1189.7
7				1190.3
6				1190.5
5				1190.5
4				1192.4
3				1194.1
T.P.	1.98	1197.87	8.98	1195.89
2				1192.10
1				1192.5
		1204.87		



	+	HI	-	E
25				1187.1
BM.			4.02	1189.97 ✓
24				1187.6
23				1186.8
22				1186.6
21				1186.8
20				1187.1 ✓
T.P.	3.19	1193.99 ✓	4.33	1190.80 ✓
19				1188.3
18				1187.2
17				1187.7
16				1188.0
15				1187.6
14				1188.0
		1195.13 ✓		

3.65 6.9
5

Spike E root 40" E/m 24 ± 50 25' Rt.

4.47 5.8 5.2 6.9 6.4 5.2 4.2 3.3 5.1
5 25 13 5 3 8 14 20

4.01 7.2
5

4.10 5.9 7.4 5.1
5 25 12

3.94 7.2
5

5.1 4.31 6.9 5.1 4.5
20 5 15 18

4.3 6.8
57K

6.0 4.59 6.1 7.9 6.4 5.8
20 5 11 8 20

4.18 7.4
5

4.42 6.3 7.1 5.8
5 9 13
25

4.36 7.5
5

4.30 6.2 6.3 7.1 5.9 5.1
5 12 5 15 20

	+	HI	−	E
37				1185.2
36				1185.1
35				1185.4
B.M	5.35			
34				1185.4
33				1184.6
T.P.	4.91	1193.09 ✓	5.74	1188.18 ✓
32				1185.5
31				1185.5
30				1185.9
29				(1186.5) 1189.3
28				(1186.4) 1189.1
T.P.	4.13	1193.92 ✓		
Quit 4:15 T.P.			4.20	1189.79 ✓
27				1188.6
26				1188.5
		1193.99 ✓		

E ℄ W 9

4.57 STK 7.9

5.34 STK. 6.5 1.5 2.5 5.8 1.3 6.3 1.0 8.2 5 8.0? 6.3 5 4.8 1.6 3.9 1.6 5.7 2.5

4.95 STK. 7.7

SPIKE West RT. 15" ELM FENCED BOW 3'±20

5.06 STK 6.0 2.5 6.0 9 7.7 6.4 7 5.0 1.7 4.1 2.0 4.9 2.5

5.25 STK 8.5

5.31 STK 6.4 3.5 7.0 1.5 8.4 7.0 7 6.2 8 5.4 1.6 6.9 3.5

5.05 STK 8.4

4.40 STK 5.8 2.5 6.0 1.1 6.6 1.4 8.0? 6.6 9 5.6 1.1 4.5 1.8 5.6 2.5

4.69 STK 7.6 7.4 9 6.2 1.0

4.07 5 5.3 2.5 4.8 E 6.3 3 7.5 8 6.3 1.6 4.7 1.9 3.2 2.5

Stake 27+0

4.20 STK 5.4 7.0 1.0

2.62 5 4.1 2.5 4.0 5 5.5 7.0 8 5.5 1.3 4.4 2.0 5.0 2.5

50				84.3
9				84.3
8				84.3
7				84.4
6				84.5 ✓
T.P.	2.76	1190.41 ✓	3.63	1187.65 ✓
5				84.7
↓				84.7
3				84.9
2				85.3
1				85.3
40				(85.1) 85.3
T.P.	2.58	1191.28 ✓	4.39	1188.70 ✓
39				85.3
38				(85.3) 85.6
		1193.09 ✓		

Lt ℄ Rt W 10

4.8 20 | 3.9 11 | 4.8 7 | 6.1 | 4.8 7 | 4.2 10 | 5.0 | 3.5 8 5.0 10 3

6.7 2 | 6.1 | 2.60 STK

5.1 20 | 5.1 9 | 6.1 | 4.7 6 | 4.5 15 | 3.21 STK

6.0 | 3.52 STK

4.4 20 | 3.9 12 | 4.5 8 | 5.9 | 4.5 5 | 3.7 7 | 4.3 15 | 2.94 STK

6.6 | 3.6 5

4.7 11 | 5.1 8 | 6.6 | 5.9 15 | 3.38 5

6.4 | 3.62 5

4.9 20 | 4.7 14 | 4.9 10 | 6.0 | 4.9 3 | 4.8 15 | 3.27 5

6.0 | 3.23 5

4.6 13 20 | 6.2 6 | 6.0 | 5.0 10 | 4.5 15 | 3.06 5

7.8 | 4.4 5

6.3 20 | 5.4 13 | 6.5 9 | 7.8 4 | 7.5 | 6.5 7 | 4.4 15 | 2.86 5

T.P.		3.53	1185.24	(1185.21)
1			82.6	
60			82.8	
9			(82.8) 83.4	
T.P	3.18	1188.77	4.40	1185.59
8			83.0	
7			83.1	
6			83.1	
5			82.8	
54			83.3	
?				
53			83.9	
52			83.9	
T.P	2.70	1189.99	3.12	1187.29
51				84.2

1190.41

E ℄ W

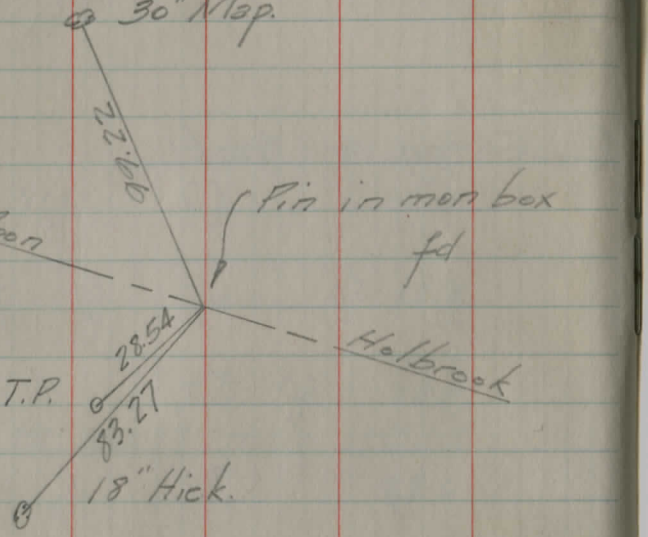
See pg 6 (rock)

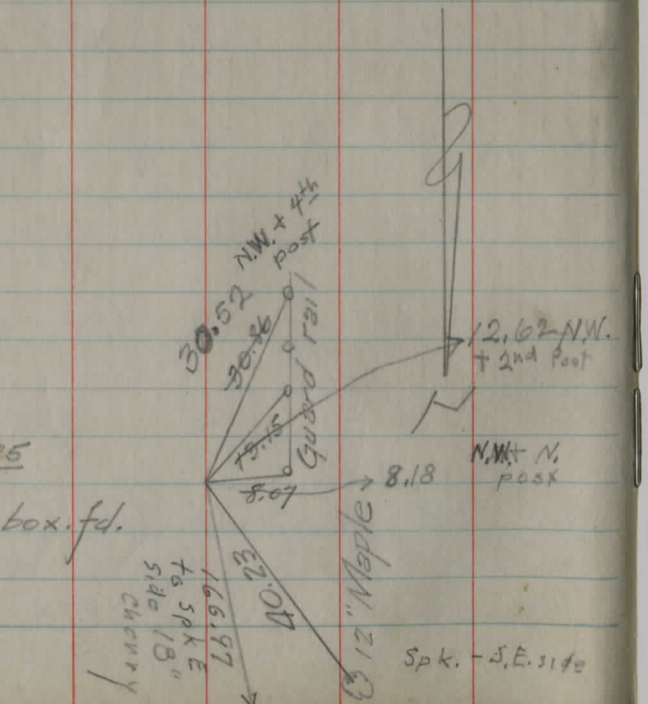
			6.2		3.08 S	
5.1 22	5.0 15		6.0	5.1 9	4.8 15	2.97 S
		6.0 4	5.4		4.17 S	
	6.3 15		7.0		5.7 15	4.40 S
			6.9	4.05 S		
5.8 15	5.8 8	2.2 2	6.9	5.6 7	3.1 15	3.44 S
			7.2		3.86 S	
	5.8 20	5.8 10	6.7	5.7 6	4.9 15	3.71 S
			6.5		3.12 S	
5.7 16	5.4 10	5.6 8	6.5	5.6 5	4.5 15	3.12 S.H.
			6.2		3.94 S	

9-12-42
Pomeroy
Clark

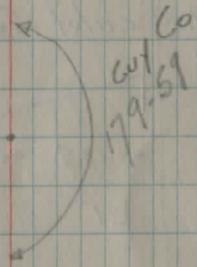
2 P.M.
TH. 188

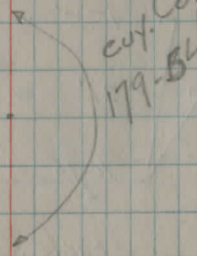
FRANKLIN STREET





(Moon road or Holbrook road northerly)





TOPO

℄

+90 22' 10" Loc
+50 20'
18"x 30' C.I.P. culvt Conc hdwls
outlet plugged O.K. otherwise
+55
← 13.5 → ← 11.5 →
+25 ≠ 21'
62+0 22'
+76 23' 14" Ch
+62 24' ℄ 8" Ch.
+50 24'
+42 28' ✓ 10" Loc
61+0 22'
+88 ≠ 21'
+84 10" Ap. 25'
+61 End gd. post 14.5'
+50 22'

brush line ± 19'

← 15.5' →
← 11.5 →
22' ← 21' →
11'
60+05 10.75 8.0
15'
back side
bridge seat

6" drain tile
61+04

Moon Rd

65+02 8" Elm 22'
+50 25
+73 ≠ 21.5'
64+07 22' ✓ 24" W.Ch
+69 21' →
+69 20.5 ✓ 24" Loc
+61 ≠ 20'
+48 20' ✓ 9" Loc
+22 21' ✓ 16" Loc
+09 21' 15" Loc
63+0 20' →

T.P.	4 7/0	118.58 ✓	2.04	113.88 ✓	
62+50				111.82	
top pipe outlet					
62				109.72	
+50					
T.P.	8.84	115.92 ✓	2.15	107.08 ✓	
+50				107.08	
C. 61+25 Next pg					
61				103.83	
+50				100.93	
60+05				99.03	
B.M.	9.23	109.23 ✓		100.00	355.

Spk 63+0

+6.0 +5.3 4.5 4.7 4.6 4.1 4.6 5.1 6.5 6.8 7.2
40 32 14.5 12 10 11.5 15.5 20 25 35

6.8
F.L. 3.9
6.6 7.0 9.2
← 3 15 50

7.05
1.25
8.3 : F.L. +3.8 +4.0
30 35

9.3 8.8 6.0 6.4 6.2 6.4 6.8 5.6 1.5 +0.8
30 16 11 10 8 10.5 11.5 21 25
25

0.1 1.8 4.4 6.5
Spike 23 20 25 30
32

1.8 2.7 2.3 2.15 2.2
10.5 8 7.5 9
10

1.4 1.2 6.0 6.6 5.8 5.4 5.6 0.0 +6.3 +7.0
25 19 13 11 10 9 25 30
30 12 40

12.6 11.4 8.0 9.1 8.6 8.3 8.7 7.4 8.1 9.0 9.8
30 22 11.5 7.5 6 9 11 16 25 30
9.5 13

10.20

S.W. 4 of S.W. wing wall

± 24' ℄ to toe of fill

± 13' ℄ to break in fill

100' ℄ of P.I.

61+25			105.51	+2.0	1.3
				37	30
T.P.	8.03	115.11	107.08		
66±10			131.90		
66+0			131.70		
65+0			126.10		1.9
					30
+50			123.40	up	4.8
					30
T.P.	8.42	131.60	123.18		
64			119.99		
±50			116.59		
T.P.	10.61	124.49	113.88		
63+0			113.88		
		118.58			

E

K1

15

0.7

40

3.8 5.0 8.7 9.7 10.4 9.9 9.6 9.9 9.6 8.9 +2.7 1.6

21 20 11.5 11 8.5 8 7 9 10 24 30

+0.3 = Summit

+0.1

2.6 2.3 6.1 5.9 6.6 5.9 5.5 5.6 +1.5

25 20 14 10.5 9 7 11 22 35

5.8 6.0 6.3 9.0 8.9 9.9 8.6 8.2 8.4 4.3 1.6 0.7

25 21 17 14 12 11.5 9 13 18 25 30

+6.2 +3.7 5.2 5.8 5.1 4.5 5.0 0.6 +2.4

35 26 12 13 9 11 8 10 17 30

+3.2 1.5 8.1 9.4 8.3 7.9 8.4 7.8 0.6 2.3 4.0

34 25 10.5 10 7 9 9.5 20 25 30

4.2 4.1 3.7 6.5 6.4 6.7 5.0 4.7 5.1 4.5 3.1 4.5 7.6

30 25 18 15 12 11 7 10 12 15 20 29

Pomeroy - Clark

GRADES VOYTKO DITCH

(Stafford road Sly)

B.M.	6.40	1198.66		1192.26	
10					
9					
8					
7					
T.P.	3.28	1199.67	2.27	1196.39	
6					
5					
4+50					
4					
T.P.	2.99	1201.65	1.01	1198.66	0.10%G
3					
2					
1					
T.P.	5.87	1203.87	3.65	1198.00	

E root 24" Elm Sta. 9+30 50' West

Ground	Grade	Rod Reading	Cut
9.54	1189.10	9.56	6.06	3.5
9.3	1189.2	9.46	5.46	4.0
8.9	1189.3	9.36	5.36	4.0
8.6	1189.4	9.26	2.26	7.0
9.6	1189.5	10.17	3.42	6.75
9.2	1189.6	10.07	2.57	7.5
	1189.65	10.02	2.02	8.0
8.8	1189.7	9.97	0.97	9.0
9.7	1189.8	11.85	3.85	8.0
9.7	1189.9	11.75	4.75	7.0
9.2	1190.0	11.65	3.65	8.0

1203.87

0+0	14' S. of ℄	S.W. stk			
"	14' N of ℄	N.W "			
"	" " " "	N.E "			
0-28	" S "	S.E "			
0-28					
T.P	6.42	1206.24	4.05	1199.82	
B.M.			3.14	1203.10	1203.10

Ch.	Grade	Rod	Reading	Cut
10.5	1190.10	13.77	5.77	8.0 ✓
10.57	1190.15	13.72	5.22	8.5 ✓
		13.72	7.47	6.25 ✓
		13.77	6.52	7.25 ✓

13.72
10.57
3.15

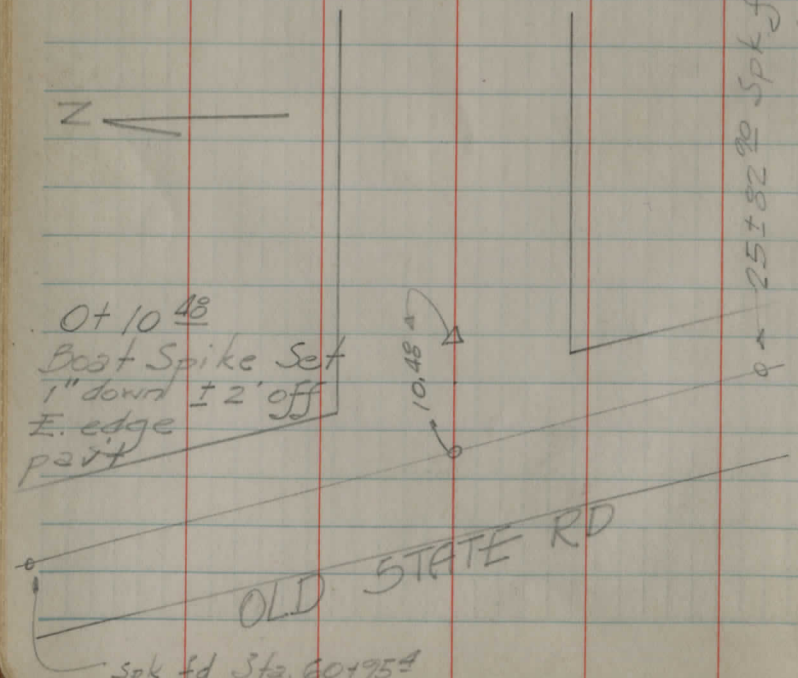
4-29-43 P.M.
Pomeroy
J. Randles
J. Radcliffe

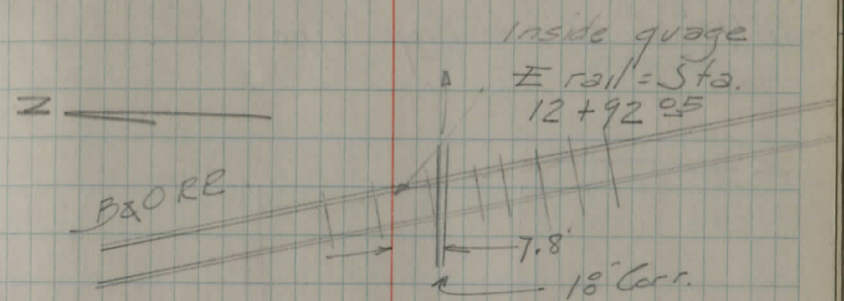
Stillwell Road
Claridon Township

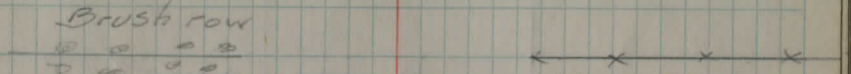
5-3-43
Pom. Hall
Randles

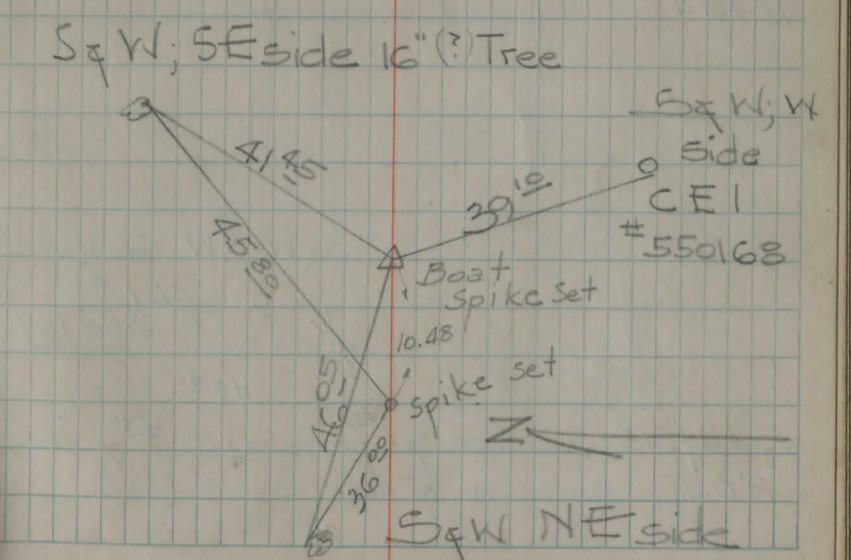
Stakes
Note: 30' Lt. (North) Sta.
30' at odd
at each

10+40 Approx Lot Line

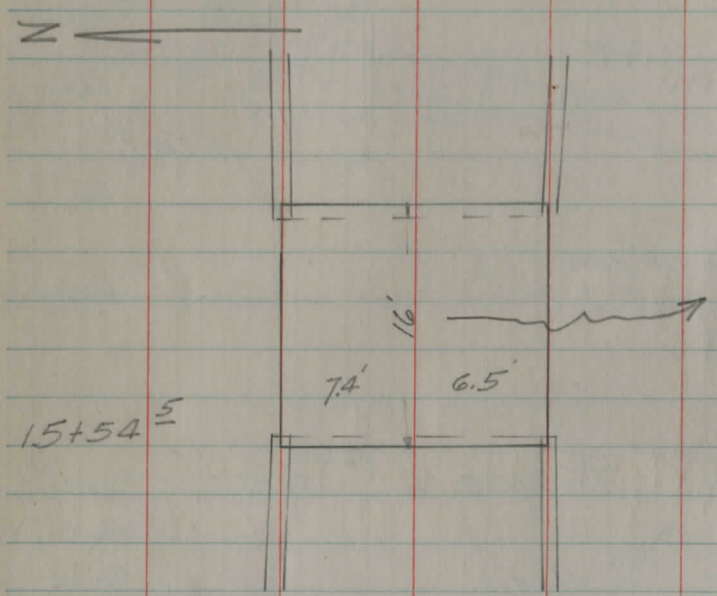








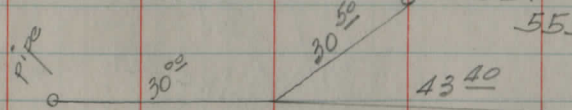
18+12.6 Prop. Line



15+54.5

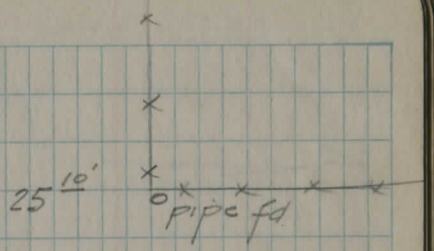
Sq W; S.W side

CE1 #553157



13+47.45 Boat Spk fd Sq W; E side

P.O.T. 10" down 12" W. Ch.



Z

39
4+44

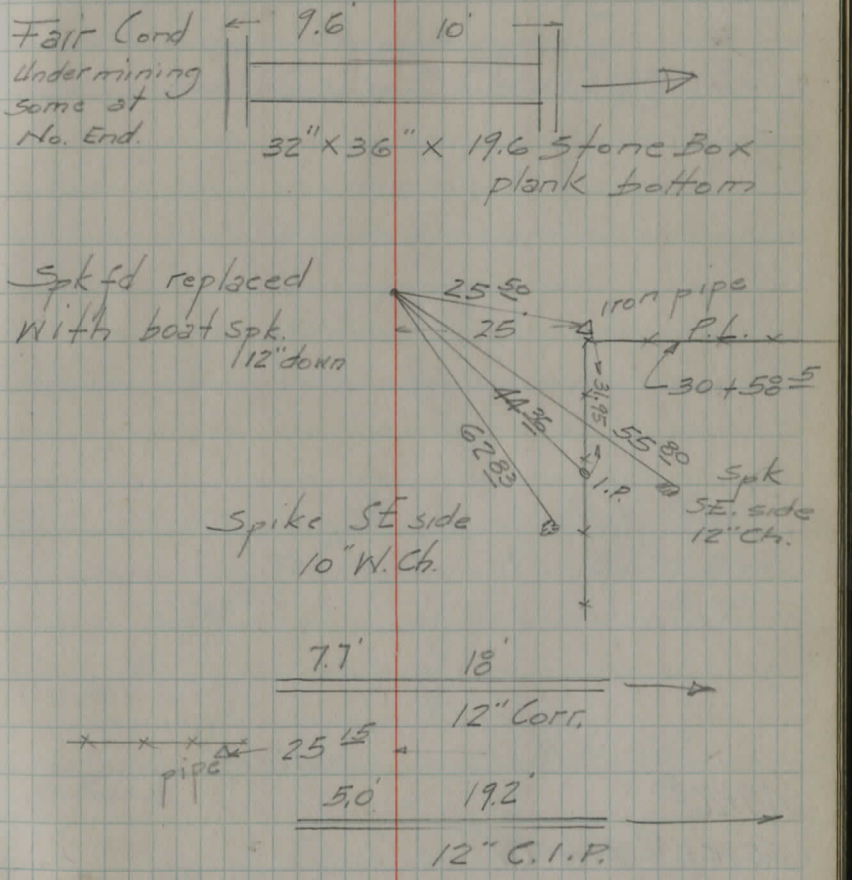
30+58.45
Δ = 0°-03' Rt.

179-57
359-54+

25+59.00 Culvt

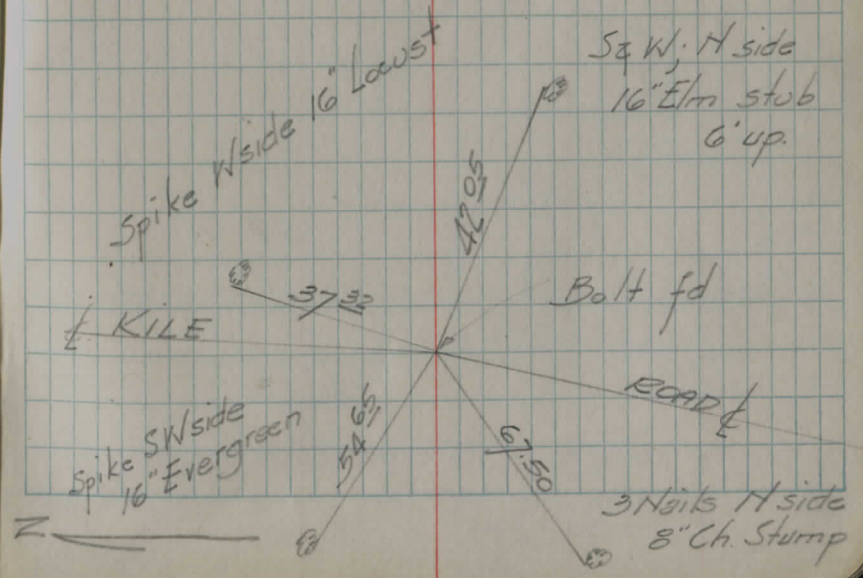
2 P.L.
Culvt

20+42.8



Note: See field book # 117 Sec. A for sections pg 121

Sec. B = FB 117 pg. 130



49+26.50
= 35+65.07 Kile Rd

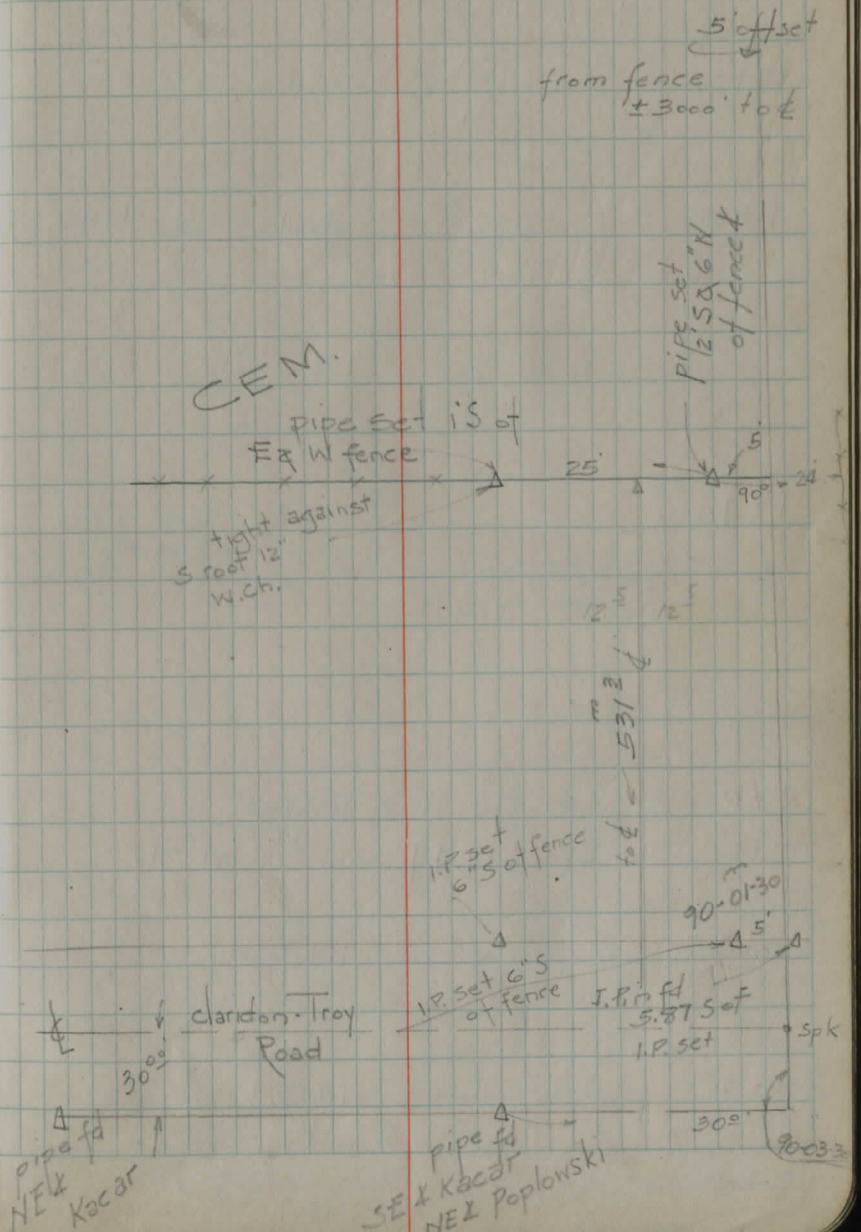
5-18-43
Port. Hall. Randles
PM part

5-19-43
Port. Hall Snyder
AM

BORTON TRUSTEES

See Pg 25
Resurvey
1944

Cemetery E of S. Steele Xing

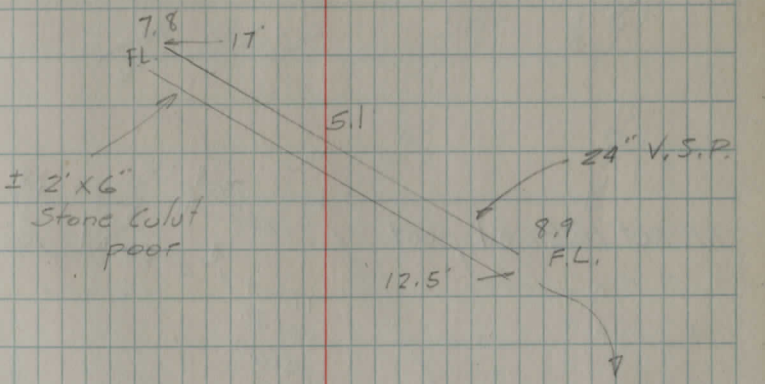


BM	7.37	107.37		100.00	Ass.
0+0			101.45		
1+0			101.1		
1+70			102.3		
2+0			103.7		
IP	10.28	117.49	0.16	107.21	
3+0			107.9		
4+0			111.5		
5+0			115.9		

NEXE Hdwall I 50 S of Tower Line

5.92

± 5.7	6.6	7.0	6.3	6.3	6.7	7.8	7.3	6.8
15	12	7	5		3	6	12.5	15

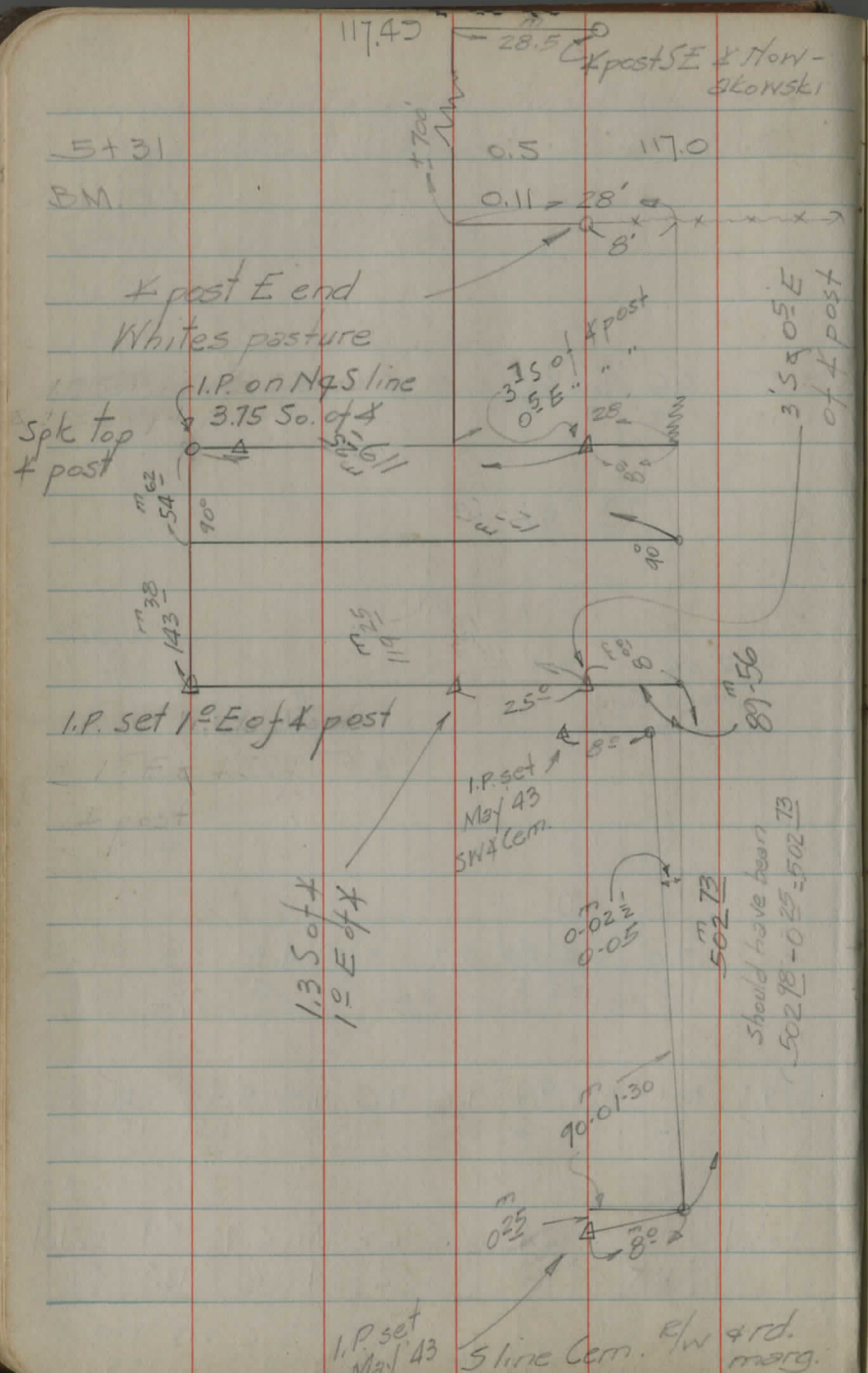


	7.0	6.6	4.0	3.7	3.9	4.3	3.3	
	15	12.5	5		3	5	12 15	

9.8	10.1	10.2	9.9	9.6	9.6	9.3	8.4	8.2
15	12	7	6		3	8	12.5	15

Level	7.0		6.4	6.0	6.2	7.0	6.4	5.9	Level
	12.5		6		2	4	6	12.5	

Lev	2.4	1.9	1.6	1.8	2.6	2.3	2.0	
	12.5			2	4	6	12.5	



I.P. N side Dr.

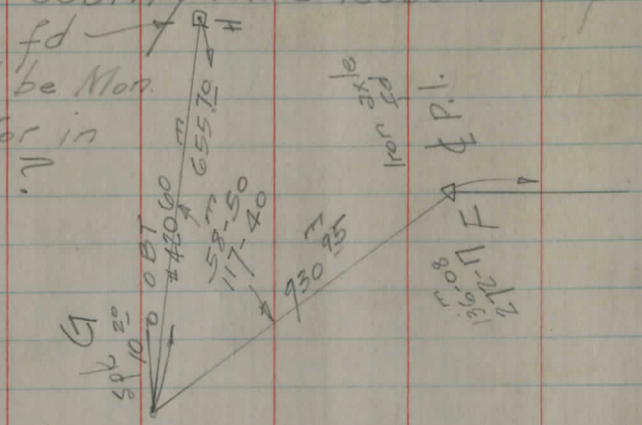
119.25
25
94.25

S 32

7-9-43 Pom - Boone

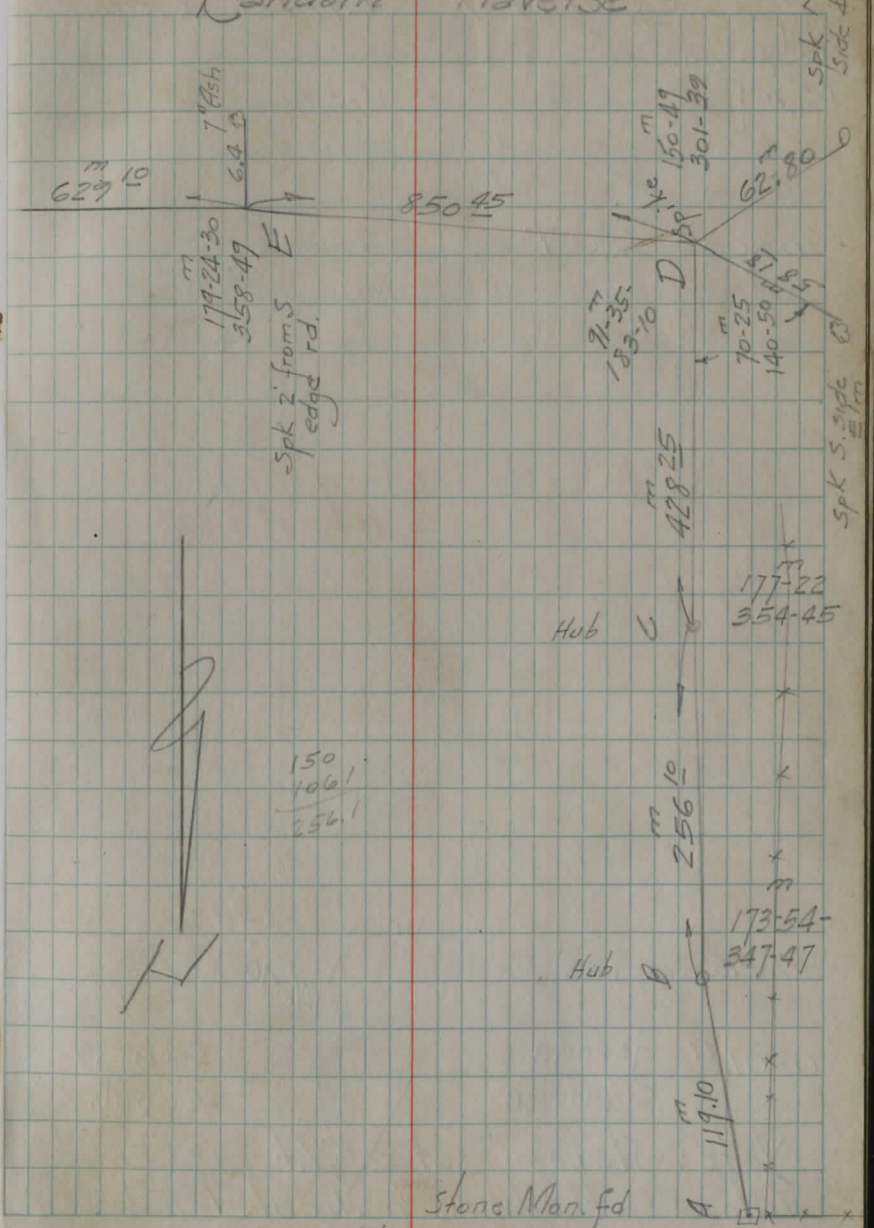
County Line Russell Twp

Stone fd
May not be Mon.
called for in
deeds ?



Spk set
27.35 from Spk
in E/m
9+04.70

Random Traverse



7-13-43 T.H. 93

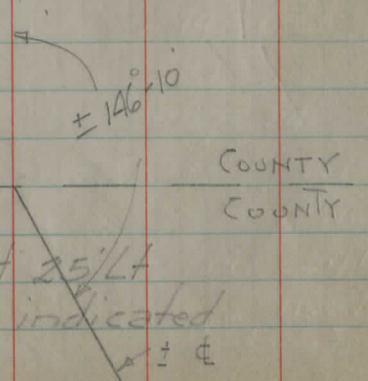
COUNTY LINE ROAD

Pott
Hall
Boone
Thompson

10+00 POT

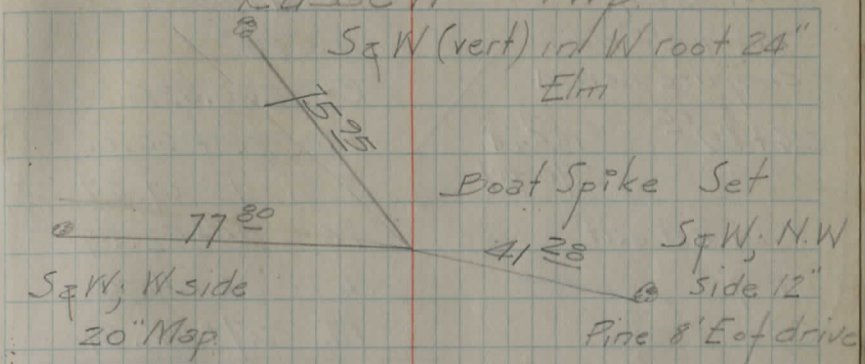
NOTE: Sta 0-01.77 to 46+67.12 is intended to be ℄ for construction only

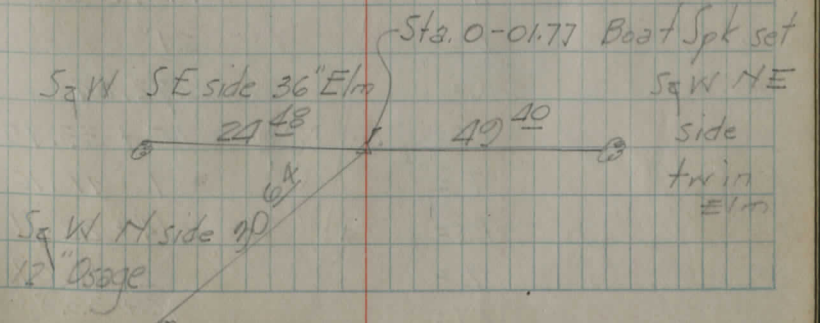
Exist. ext. = 8'



Note: Stakes set 25' Lt unless otherwise indicated

Russell Twp.





Note: 32+59.50
swung 2.00 W
Compute new Δ
26+60.06
135-04
270-09
15 Ext. exit.
New

Δ=	44-55-30 Lt.
D=	22°
R=	260.435
P.I.	26+60.06
T	1 07.67
PC	25+52.39
L	204.20
P.T.	27+56.59

Δ	45-07
D:	22
R:	260.435
P.I.	26+60.06
Check → T	1 08.19
P.C.	25+51.87
L	2 05.08
P.T.	27+56.95
E=	21.58

15+33.95

Δ=	44-20 Lt
D=	21°
R=	272.84
P.I.=	15+33.95
T=	1 11.16
PC=	14+22.79
L=	2 11.09
PT=	16+33.88

0-07
0-18
To random pt. E

S&W; E side 28" Apple

47.61	Def
26+0	= 5°-14-15
27+0	= 16-14-15
PT	= 22-27-45

31.45

Boat Spike set

63.88

82.40

S&W E side Elm

S&W; S.E. side 10" Ash

Sta	Def
26	5-17-40
27	16-17-40
+56.95	22-33-30

See pg. 29 for Lot 4

S&W; N root 20" Cucumber

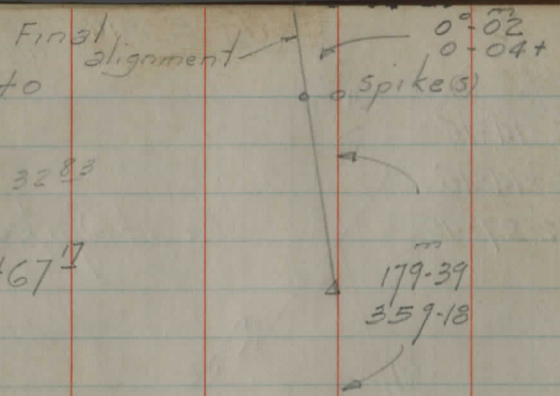
19.08

Iron Axle fd

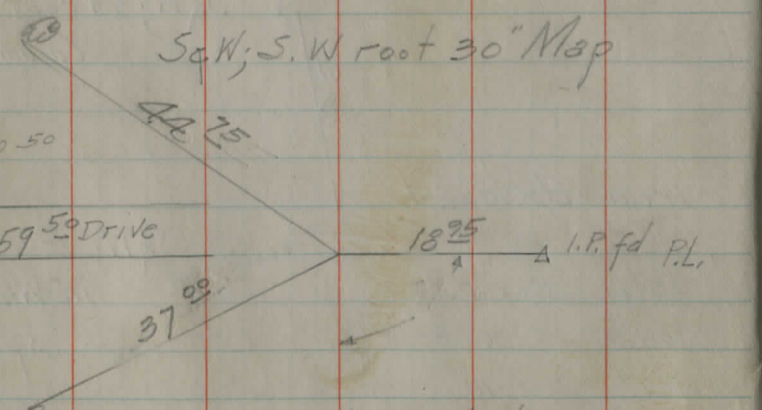
Sta	Def
15+0	8-06-30
16+0	18-36-30
P.T.	22-10

34.00

S&W; E side 10" White spruce



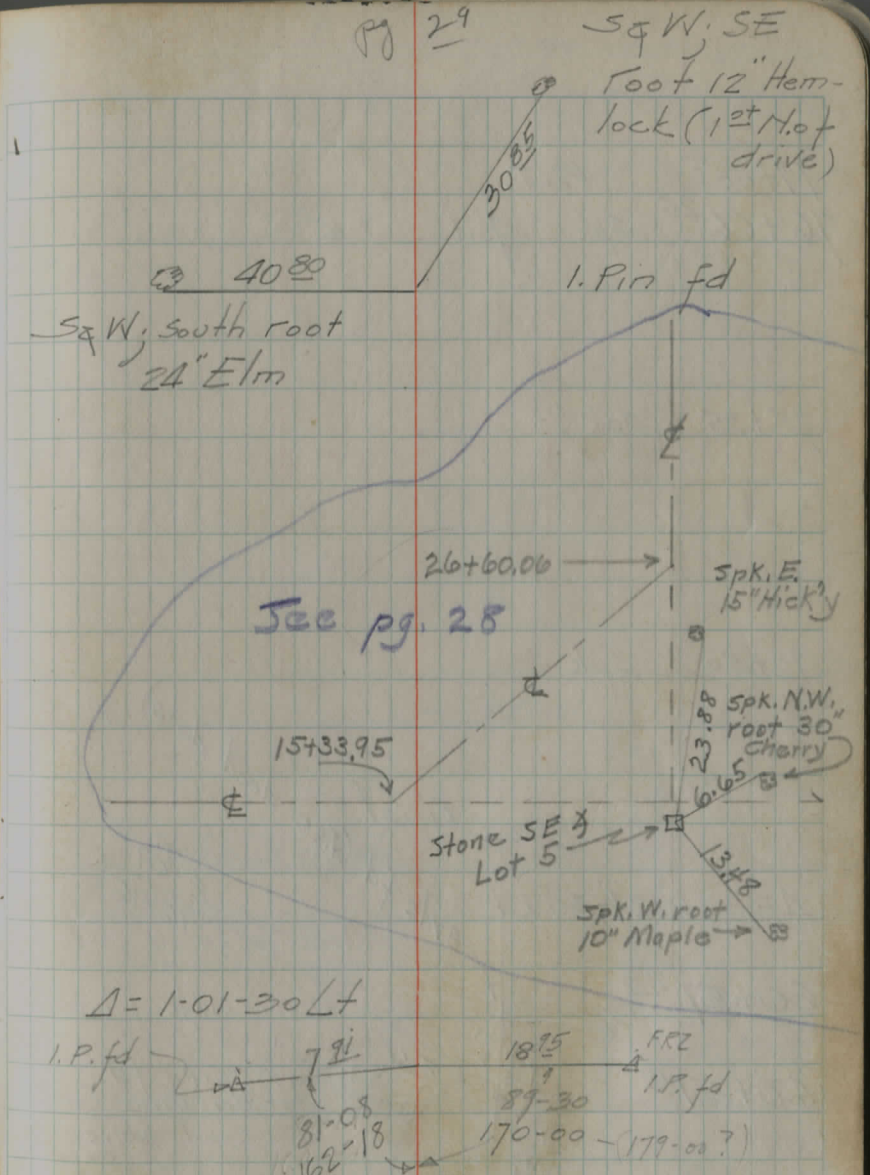
Note:



Sq W NW root 38" Maple

32+0 Stks set 25' Rt

Pg 29



79+00 POT

76+66.25 Spk Quit 7-16

75+35 Spk

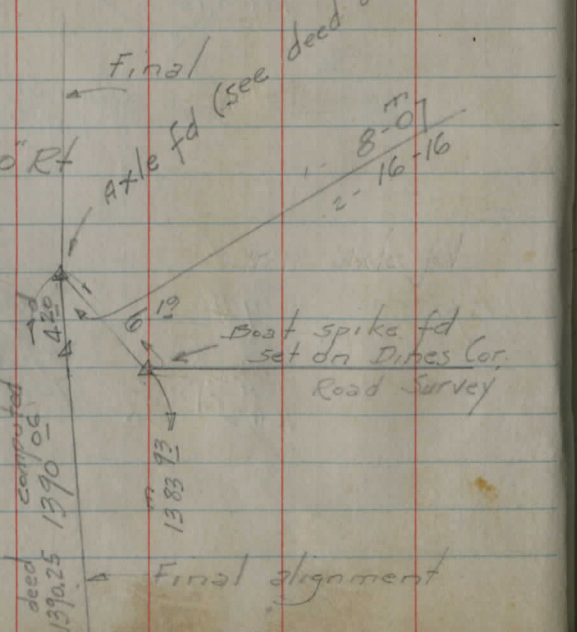
70+50 Spk

42.77

Δ = 0°-24-30" Rt

60+57.23

60+51.19



Sq W E root
14" Map

Sq W E side
middle (3) Ash

106.70
54.60

Boat Spike Set

Sq W CEI
SE side 29.50
245228

Final

Spike 5" Maple

Δ = 179-35
Δ = 359-11

59.25

12.82

Cleve. Regional
Sur. Mon.

69.03
34.01

Spike SE side CEI pole # 257924

Spike 5" Elm

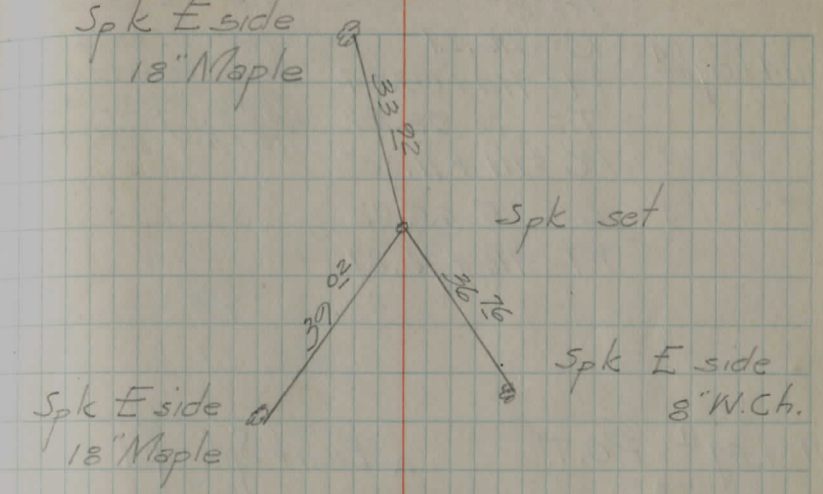
Final

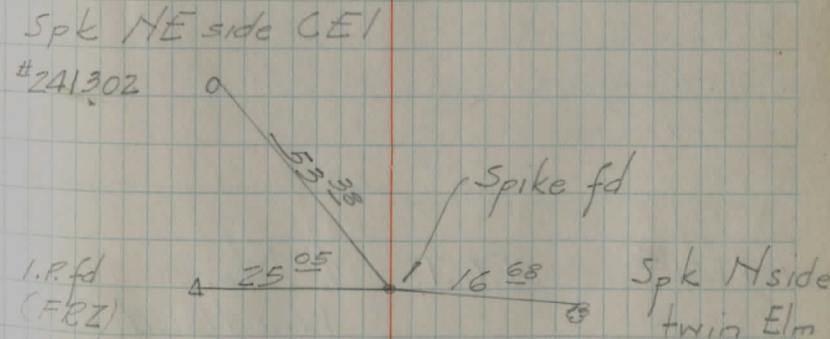
74+84.55 P.O.T.

89+55.05

179-59
359-58+

8955.05
6057.23
2897.82





Δ = 45-14-30 Rt
D = 8°
R = 716.21
PI = 114+09.84
T = 298.49
PC = 111+11.35
L = 565.52
PT 116+76.87

114+09.84

111+59.11 P.O.T. △ Boat Spk fd

48 ot

104+51.96 P.O.T. ℄ No. Woodland Rd.

112+0 - 3°-32'-45
113+0 - 7-32-45
114+0 11-32-45
115+0 15-32-45
116+0 19-32-45
116+76.87 22-04-30

S&W; NE side 12" W. Ch. 32

53.21

30.08

I.P. fd

S&W; S side Osage

Spike NE side 28" Elm

33.25

26.55

S&W S side 10" W Ch

S&W; E side 14" Maple

Cleve. Regional Geodetic Survey mon.

55.67

30.04

Bit. Mac.

Bit. Mac.

B.R. spike set from ref.

32.58

Bent Spk &W; SE side 12" Map

43.12

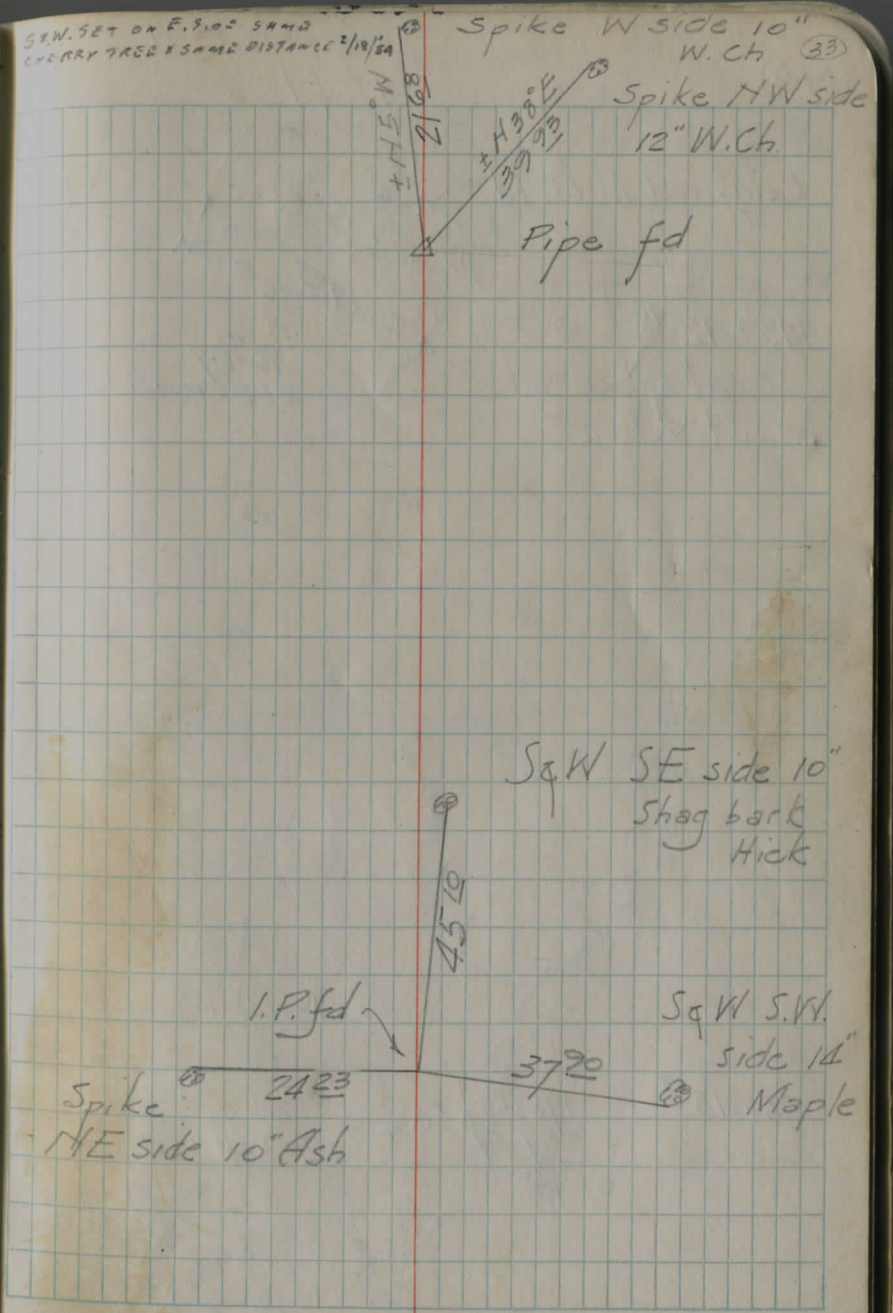
S&W; NW side

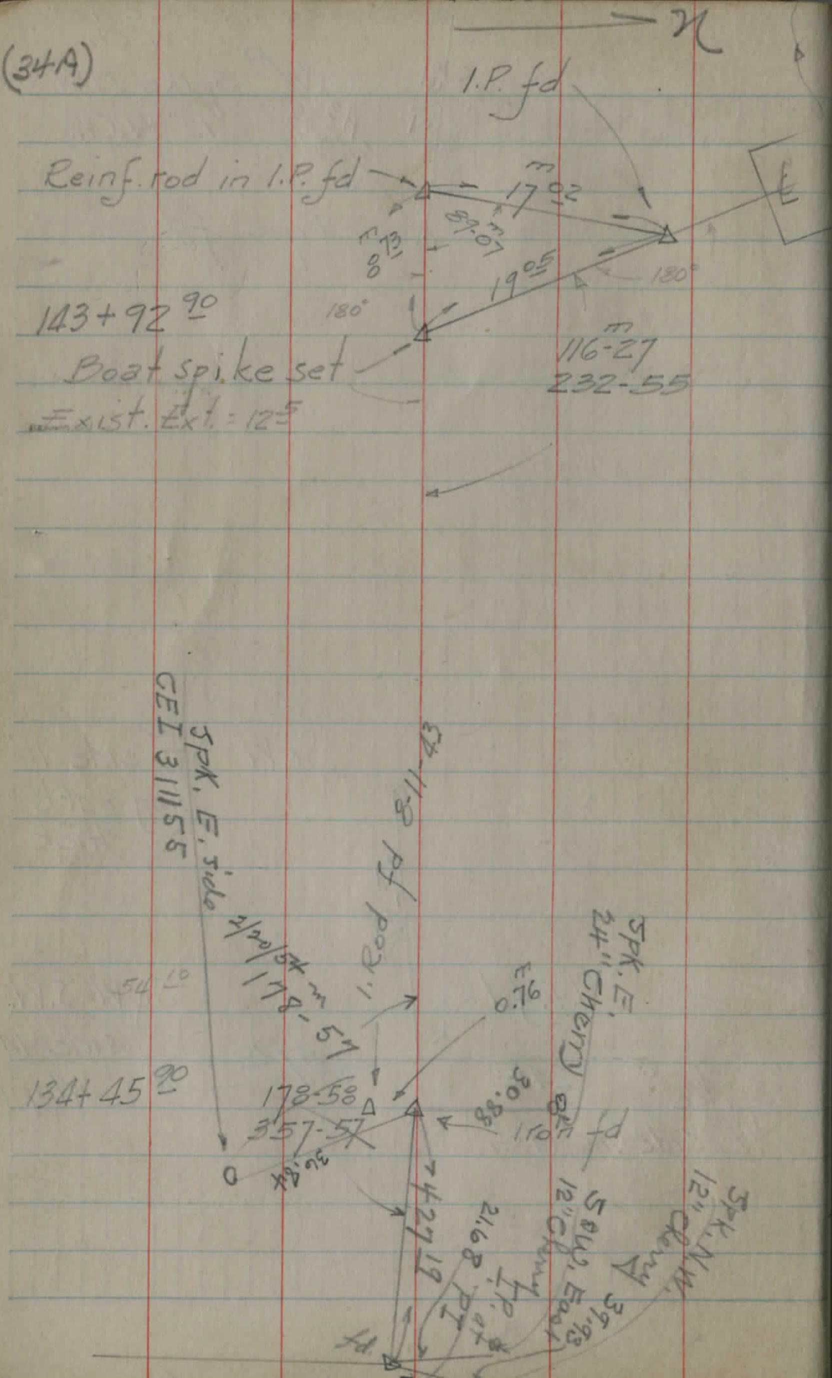
132+00.12

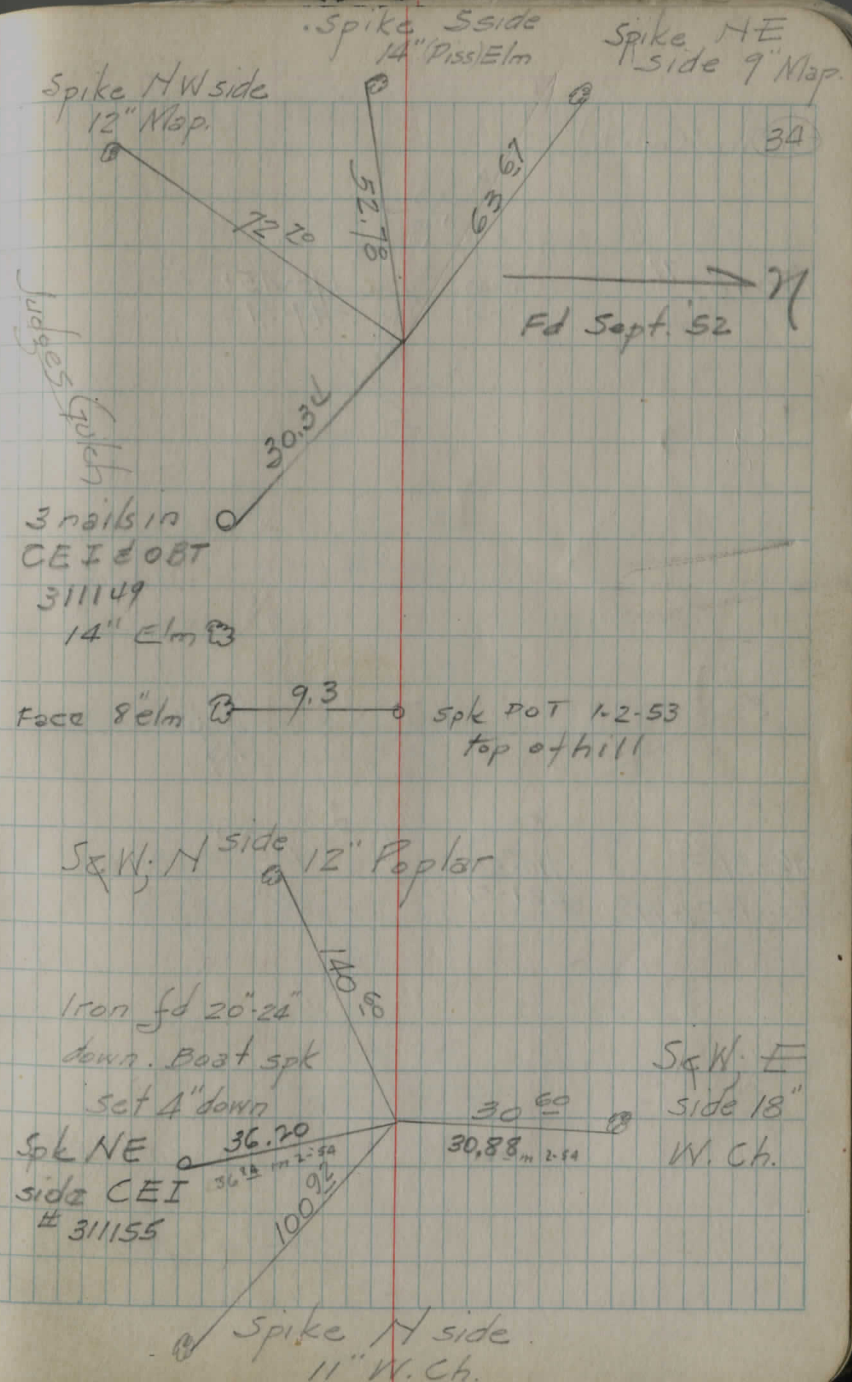
Δ = 89-33-20 Lt
D = 13-18-32
R = 430.51
PI 132+00.19
T 4 27.19
PC 127+73.00
L 6 72.90
PT 134+45.90

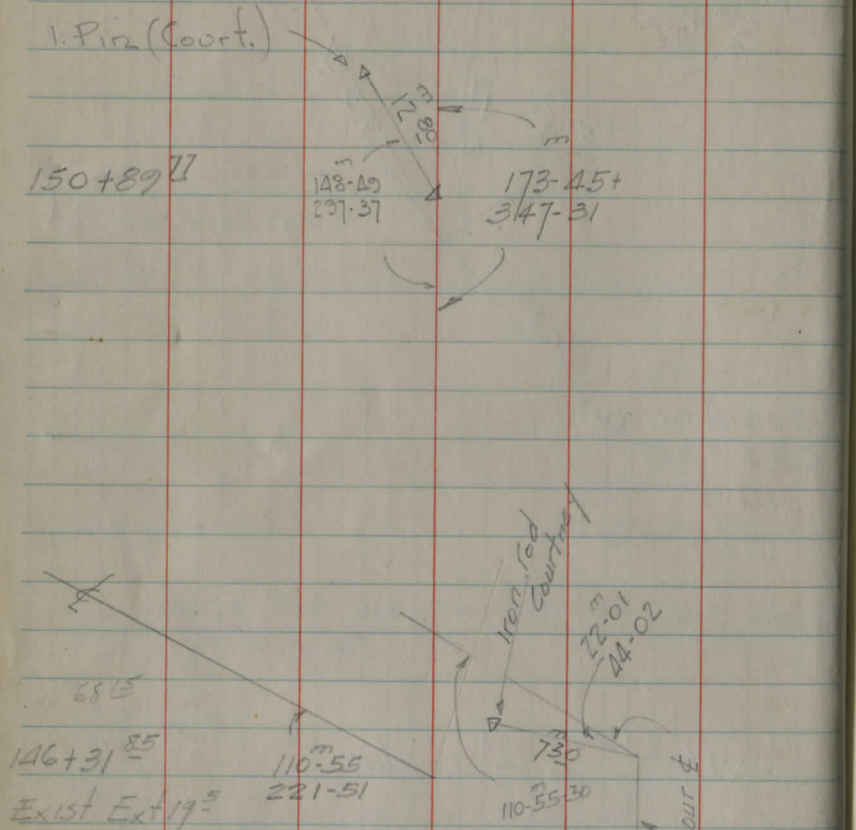
119+79.92

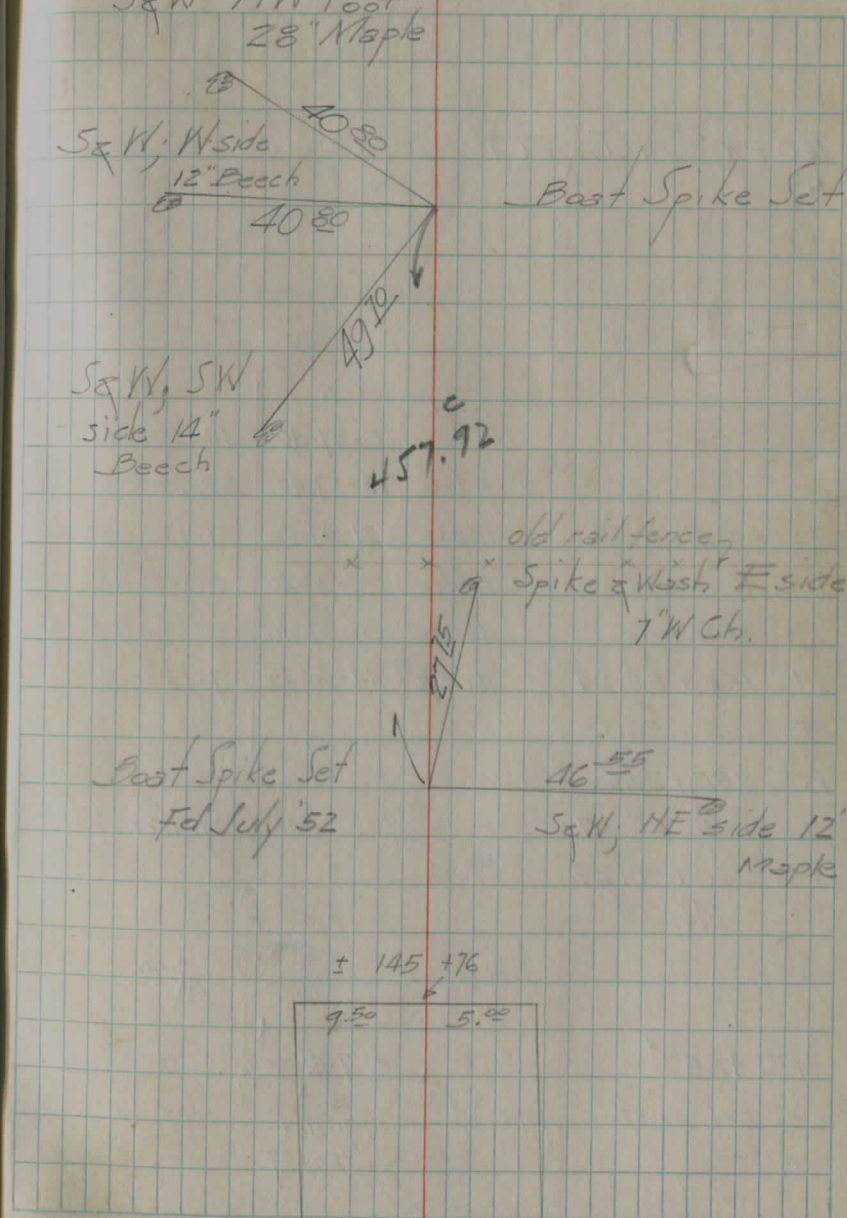
Δ = 45°-14-30 Lt
D = 8°
R = 716.21'
PI = 119+79.92
T = 2 98.49
P.C. = 116+81.43
L = 5 65.52
P.T. 122+46.95




N
I.P. fd
Reinf. rod in I.P. fd
17.02 m
89.07 m
8.73 m
19.05
180°
180°
143+92.90
Boat spike set
116-27 m
232-55
Exist. Ext. = 12.5
Spk. E. side CEI 311155
2/20/57 m 178-57
I. Rod fd 8-11-43
0.76 m
Spk. E. 24" Cherry
134+45.90
178-58
357-57
30.88
38.88
Iron fd
74.27
Spk. N.W. 12" Cherry
Spk. W. E. 12" Cherry
fd.


Spike S side 14" (Piss) Elm
Spike NE side 9" Map.
Spike NW side 12" Map.
72.70
52.70
63.67
N
Fd Sept. 52
Judges Gulch
30.30
3 nails in CEI & OBT 311149 14" Elm
Face 8" elm
9.3
spk POT 1-2-53 top of hill
S&W; N side 12" Poplar
140.18
Iron fd 20"-24" down. Boat spk set 4" down
S&W. E side 18" W. Ch.
30.60
30.88 m 2-54
36.20
36.14 m 2-54
Spk NE side CEI # 311155
100.92
Spike N side 11" W. Ch.


1. Pin (Court.)
12.80
148-49
297.37
173-45+
347-31
150+89
Iron rod (Courtney)
12-01
44-02
7.30
110-55-30
our ℄
68
146+31
110-55
221-51
Exist Ext 19


S & W HW root
28" Maple
40.80
S & W, W side
12" Beech
40.80
Boat Spike Set
49.70
S & W, SW
side 14"
Beech
457.72
old rail fence
Spike & Washer E side
7" W Ch.
27.15
Boat Spike Set
Ed July '52
46.55
S & W, NE side 12"
Maple
± 145 +76
9.50
5.00
7'
7'
± 145 +42

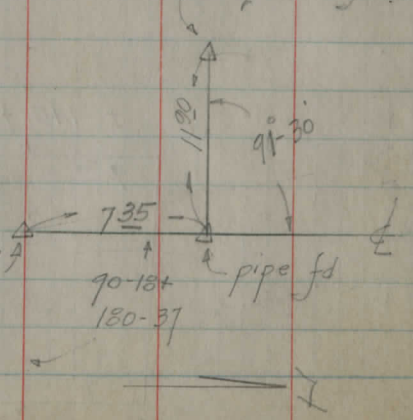
9 77

160+90.23 P.T. & POT

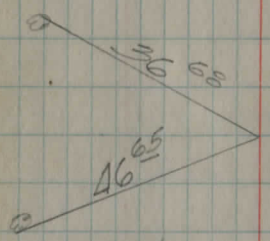
	For.	Back.
70.34		
156+0	5-37-40	44-50-45
157+0	13-37-40	39-13-05
158+0	21-37-40	31-13-05
159+0	29-37-40	23-13-05
160+0	37-37-40	15-13-05
160+90.23	44-50-45	7-13-05

Δ = 89°-41'-30" Rt.
D = 16°
R = 358.10'
PI 158+85.84
T 3 56.18
PC 155+29.66
L 5 60.57
PT 160+90.23
E. = 146.98

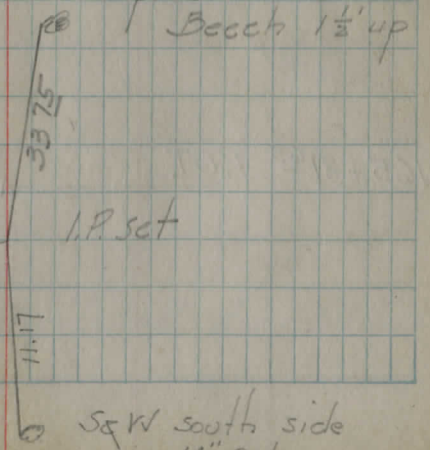
158+85.84
42' Ext. exist pipe Set
try 85



S & W NE side 8" Elm



S & W
S side twin Whitewood
± 3' W of fence



168+01 37 POT ○ Spike set

68 35

Russel-Chester Twp. line (per FR7)

165+31 65 P.O.T.

12'-14' Bit Mac.

± 9.75' ± 4'

Note: ℄ hits ctr of trav. rd ± 2.50' Rt

HE cor. Conc. Sign (largest square)

70 82 ±

S & W S side 24" W. Ch. (twin)

43

24 80

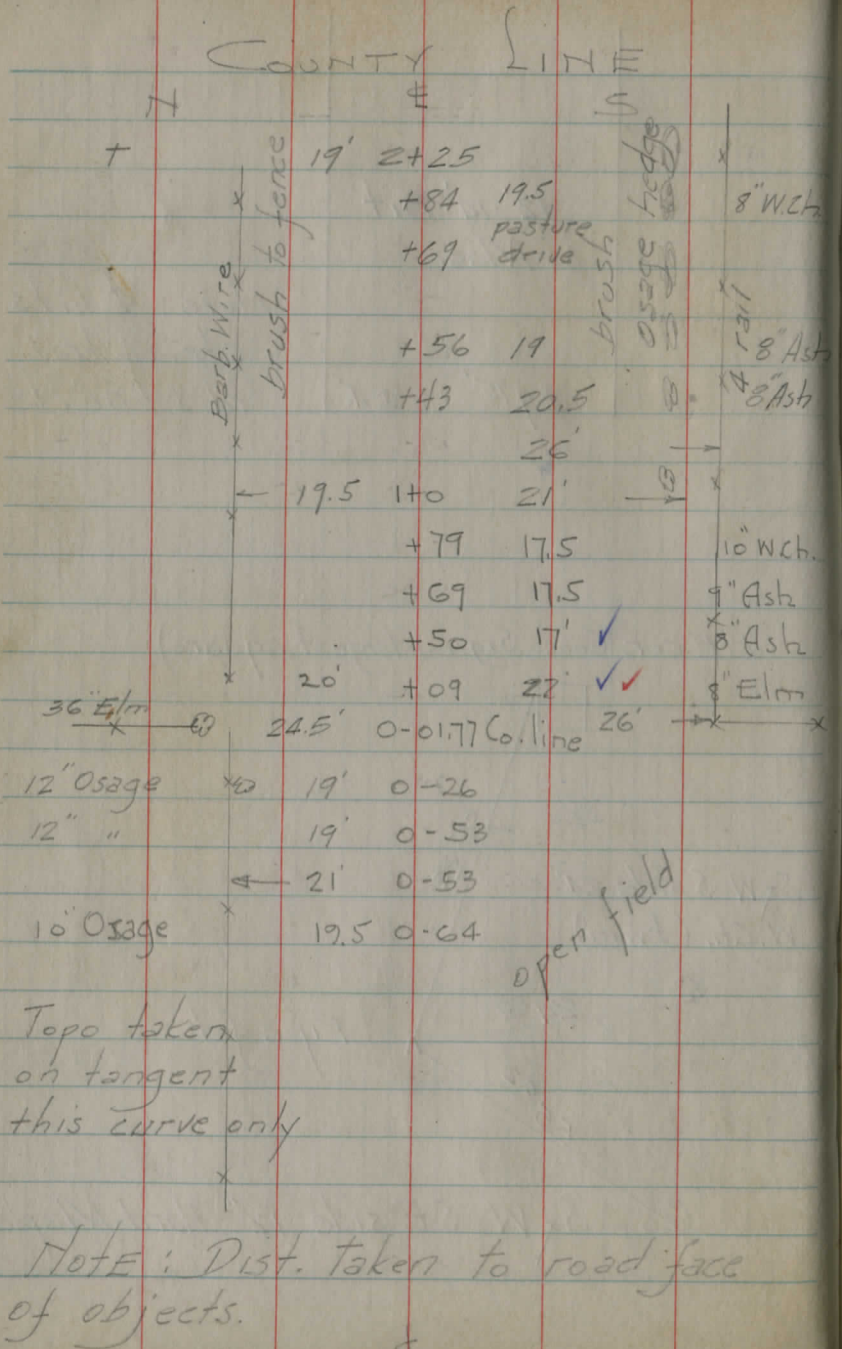
Pipe fd

62 ±

55

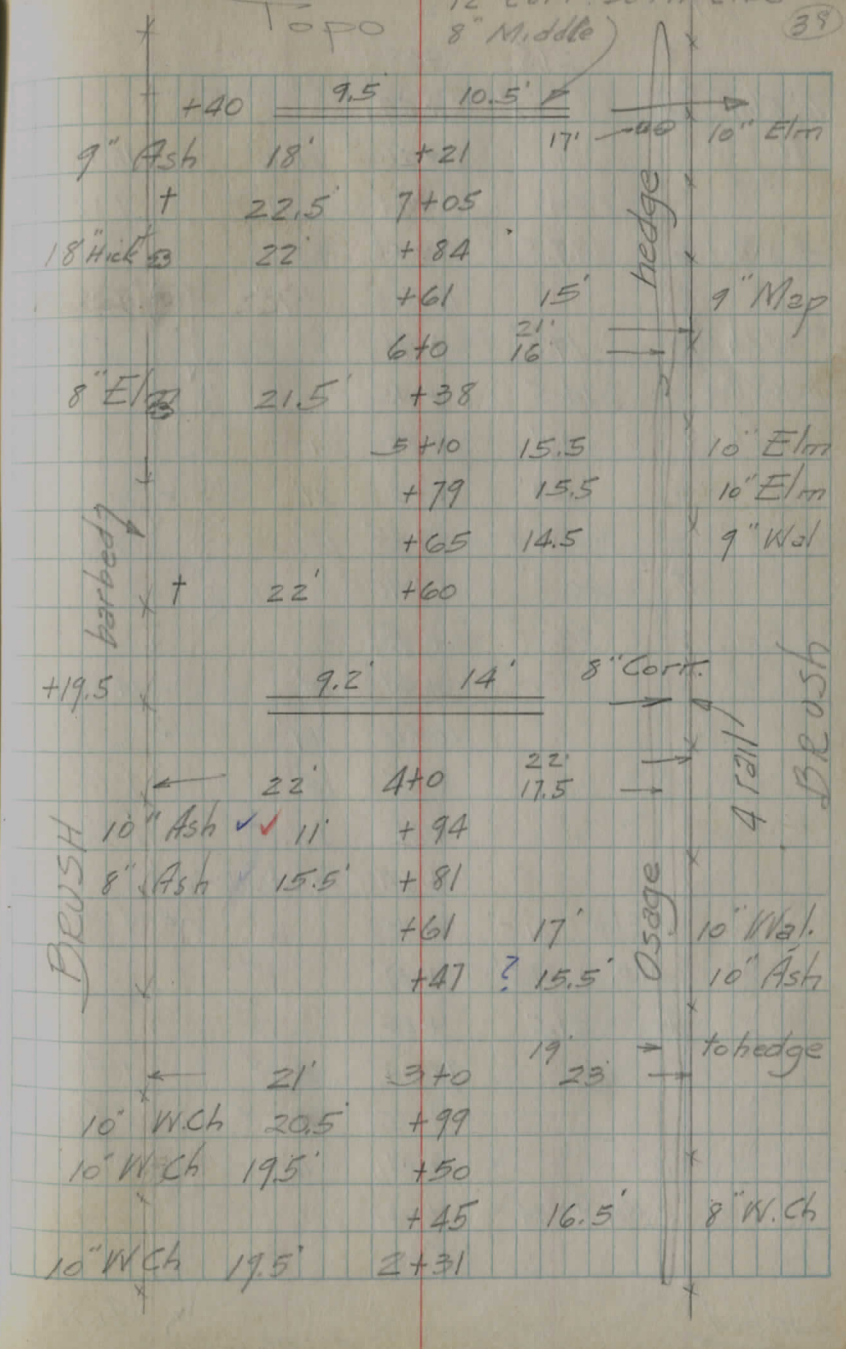
68

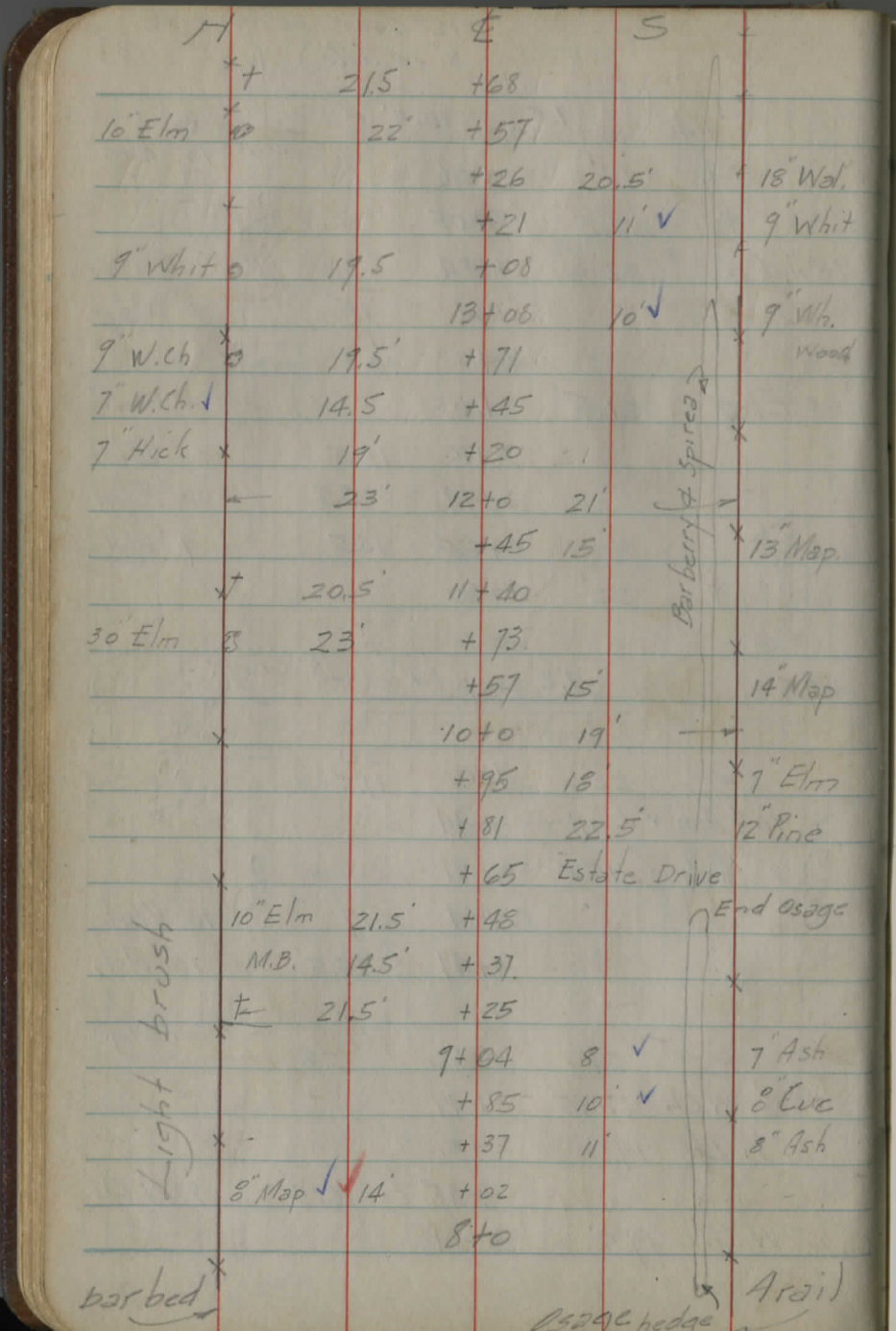
S & W SE side 12" Hard Maple

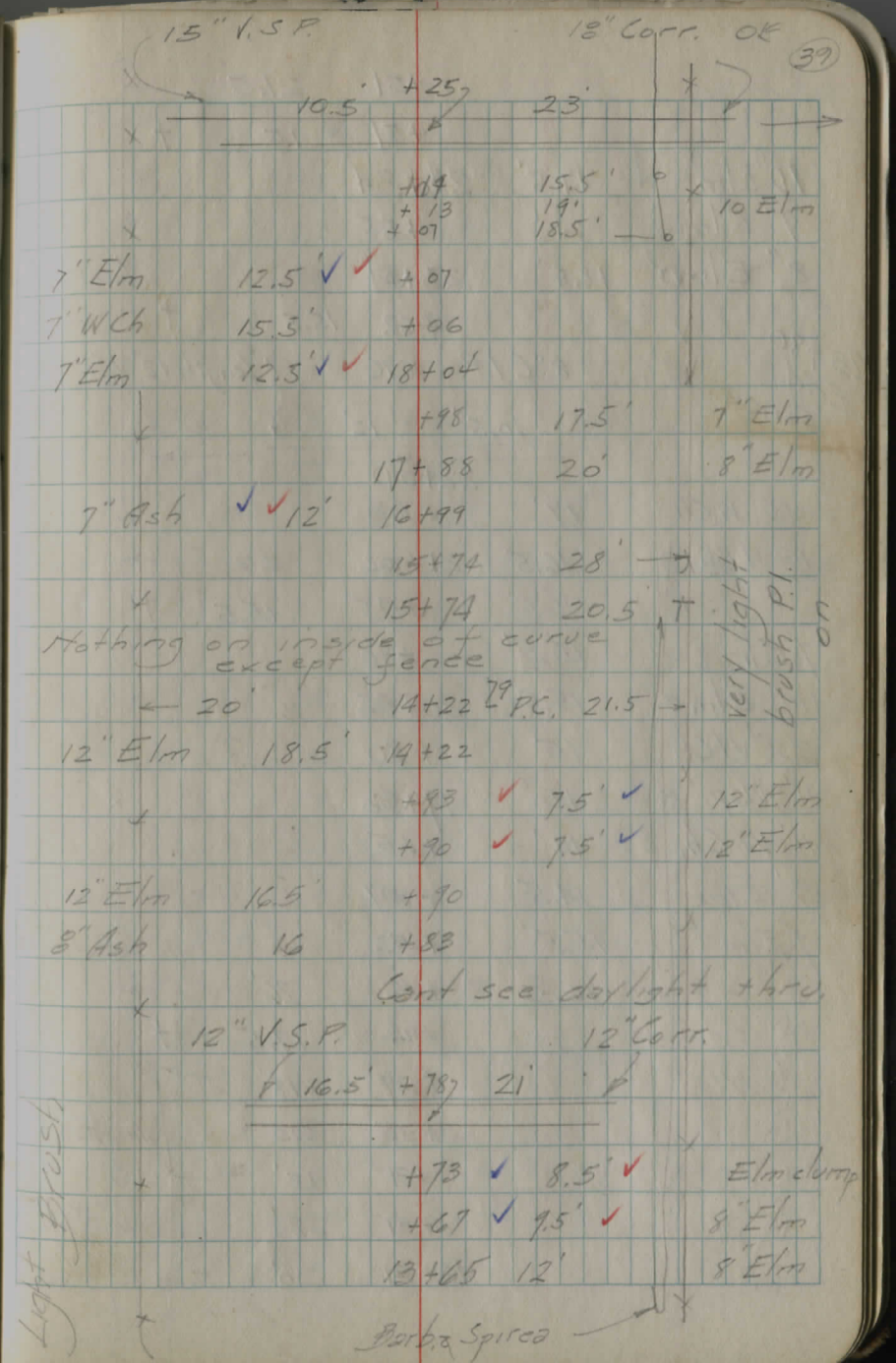


Topo taken on tangent this curve only

Note: Dist. taken to road face of objects.



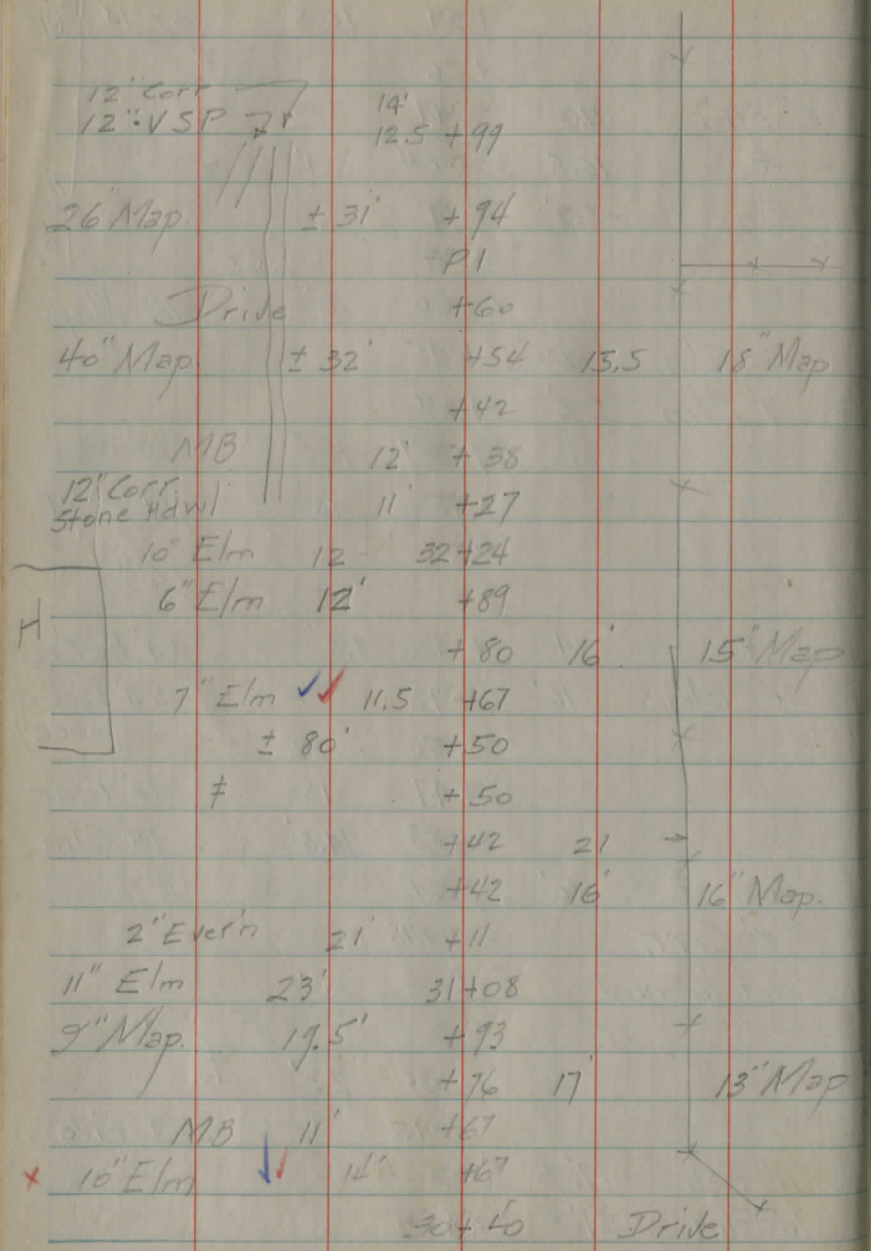

M
C
S
21.5'
+68
10" Elm
22'
+57
+26
20.5'
18" Wal.
+21
11'
9" Whit
9" Whit
19.5'
+08
13+06
10'
9" Wh.
Wood
9" W.Ch
19.5'
+71
7" W.Ch.
14.5'
+45
7" Hick
19'
+20
23'
12+0
21'
+45
15'
13" Map
20.5'
11+40
30" Elm
23'
+73
+57
15'
14" Map
10+0
19'
+95
18'
7" Elm
+81
22.5'
12" Pine
+65
Estate Drive
10" Elm
21.5'
+48
End osage
M.B.
14.5'
+31
21.5'
+25
9+04
8'
7" Ash
+85
10'
8" Cuc
+37
11'
8" Ash
8" Map
14'
+02
8+0
Barberry & Spirea
Light brush
barbed
Osage hedge
Rail

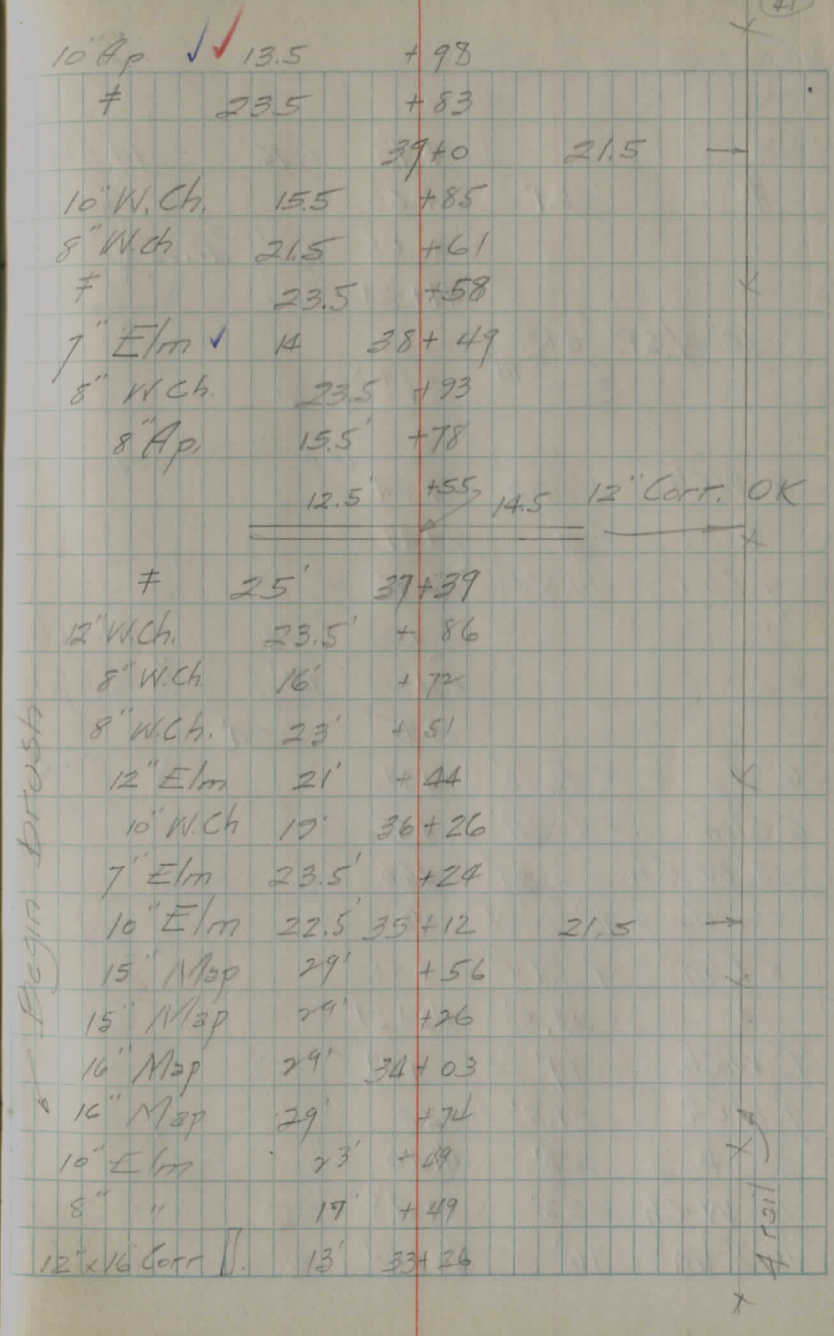

15" V.S.P.
18" Corr. CF
39
10.5'
+25
23'
+19
15.5'
+13
19'
10 Elm
+07
18.5'
7" Elm
12.5'
+07
7" W.Ch
15.5'
+06
7" Elm
12.5'
18+04
+98
17.5'
7" Elm
17+88
20'
8" Elm
7" Ash
12'
16+99
15+74
28'
15+74
20.5'
Nothing on inside of curve
except fence
20'
14+22 PC.
21.5'
12" Elm
18.5'
14+22
+93
7.5'
12" Elm
+90
7.5'
12" Elm
12" Elm
16.5'
+90
8" Ash
16
+88
Can't see daylight thru
12" V.S.P.
12" Corr.
16.5'
+78
21'
+73
8.5'
Elm clump
+67
9.5'
8" Elm
13+65
12'
8" Elm
Very light brush on
Light brush
Barb. Spirea

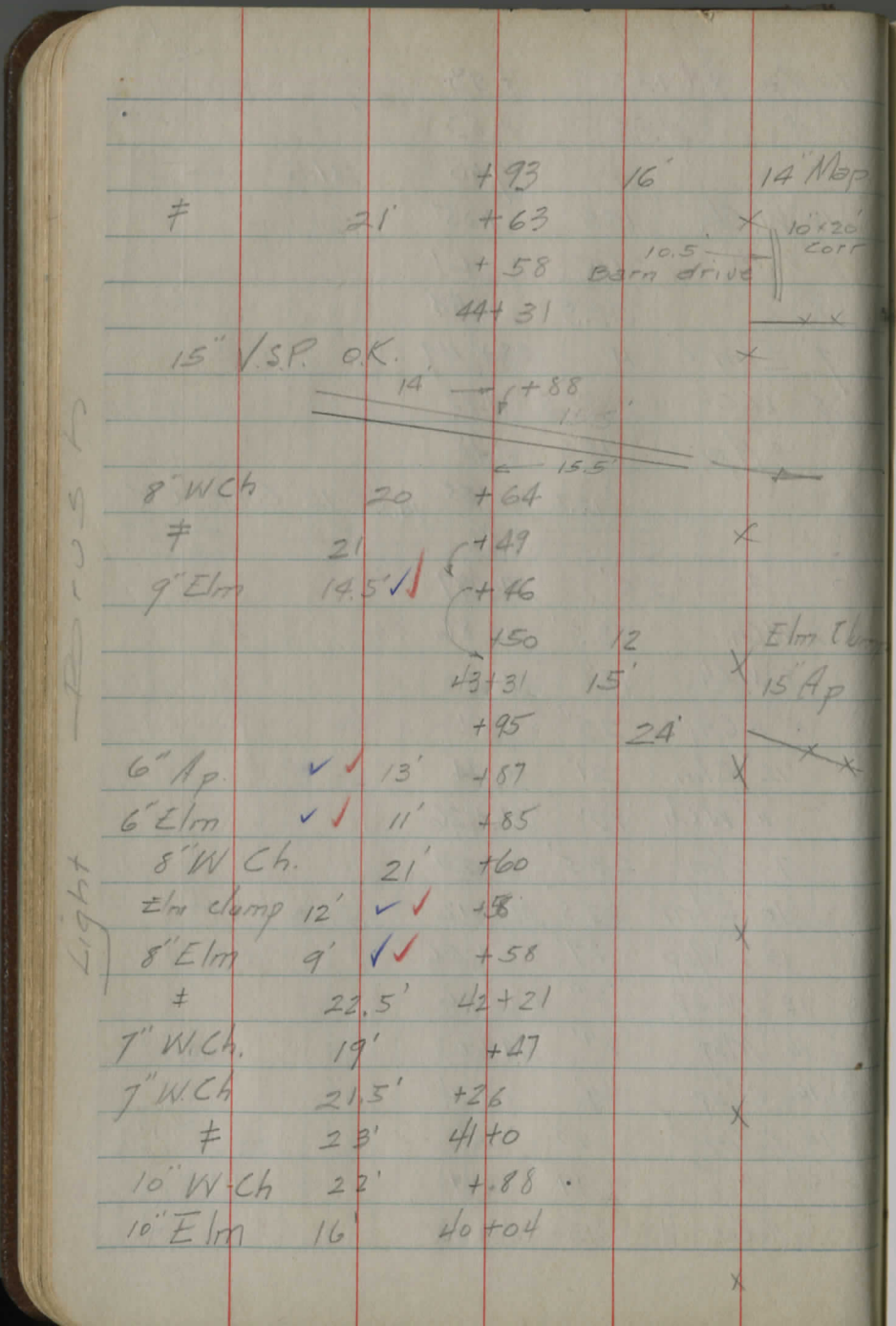
		+51	21.5	
		+51	15	
10" Elm	17.5'	24+34		
9" Elm	21'	+55		
8" Elm	18.5'	23+07		
		+62	15.5	
23+80 End fence	8" C.I.P	OK	1 Length 12" VSP	
	10.5'	12'		
		22+04		
15" W Ch	17'	+63		
15" W Ch	16.5	21+02	22	
		+75	15.5'	
7" Elm	15.5'	+70		
10" Elm	15.5'	20+36		
28" W Ch	15	+80		
11" Map	15'	19+38		
11" W Ch	14'	+65		
9" Elm	14.5	+57		
7" Elm	15.5'	+52		
	16.5	+46	26'	
		+46	19.5'	
		+37	18'	
		+35	22	10" Elm
		+31	15'	
		+31	22'	10" Elm
		18+31	20'	10" Elm

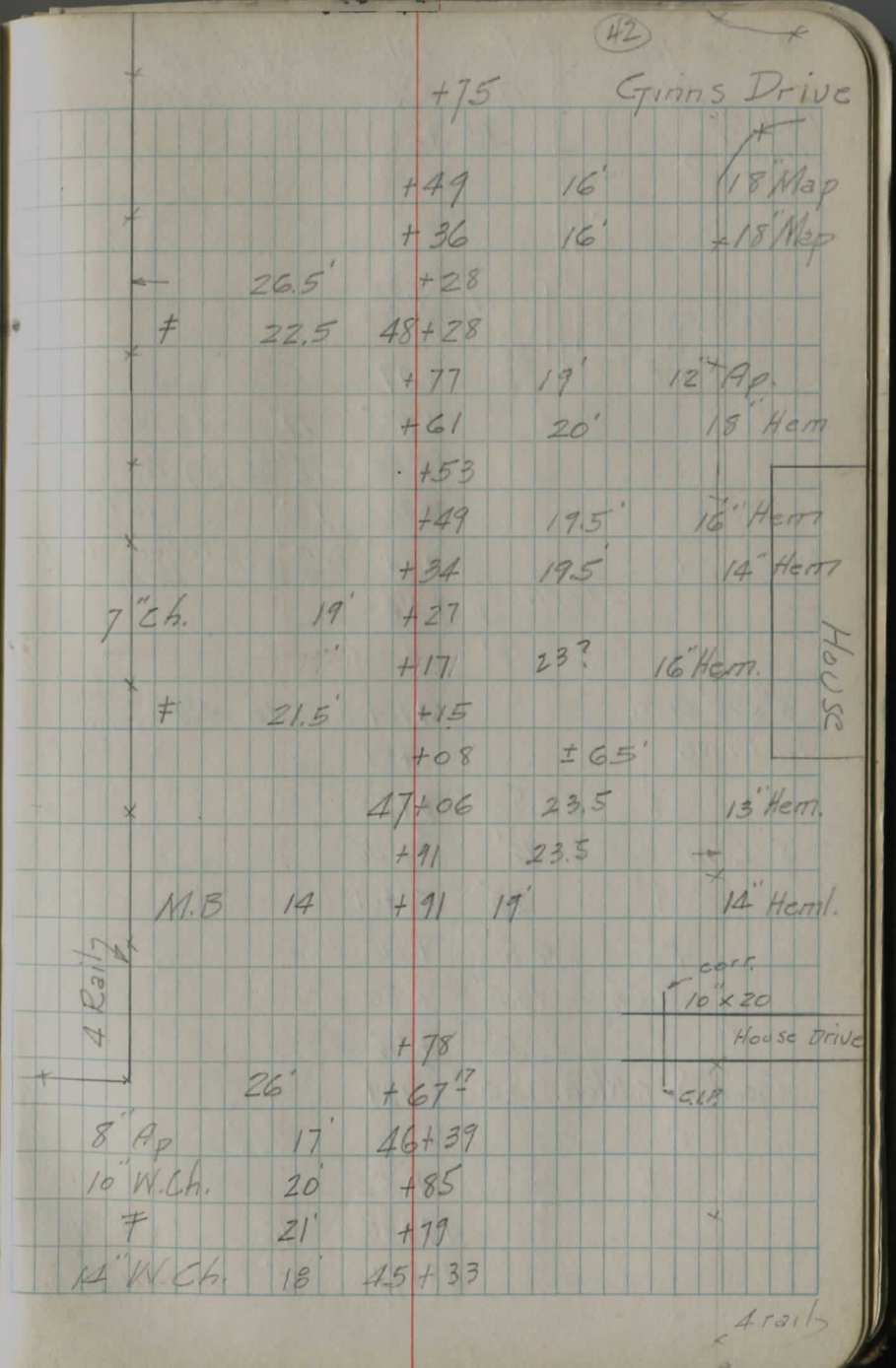
Light brush

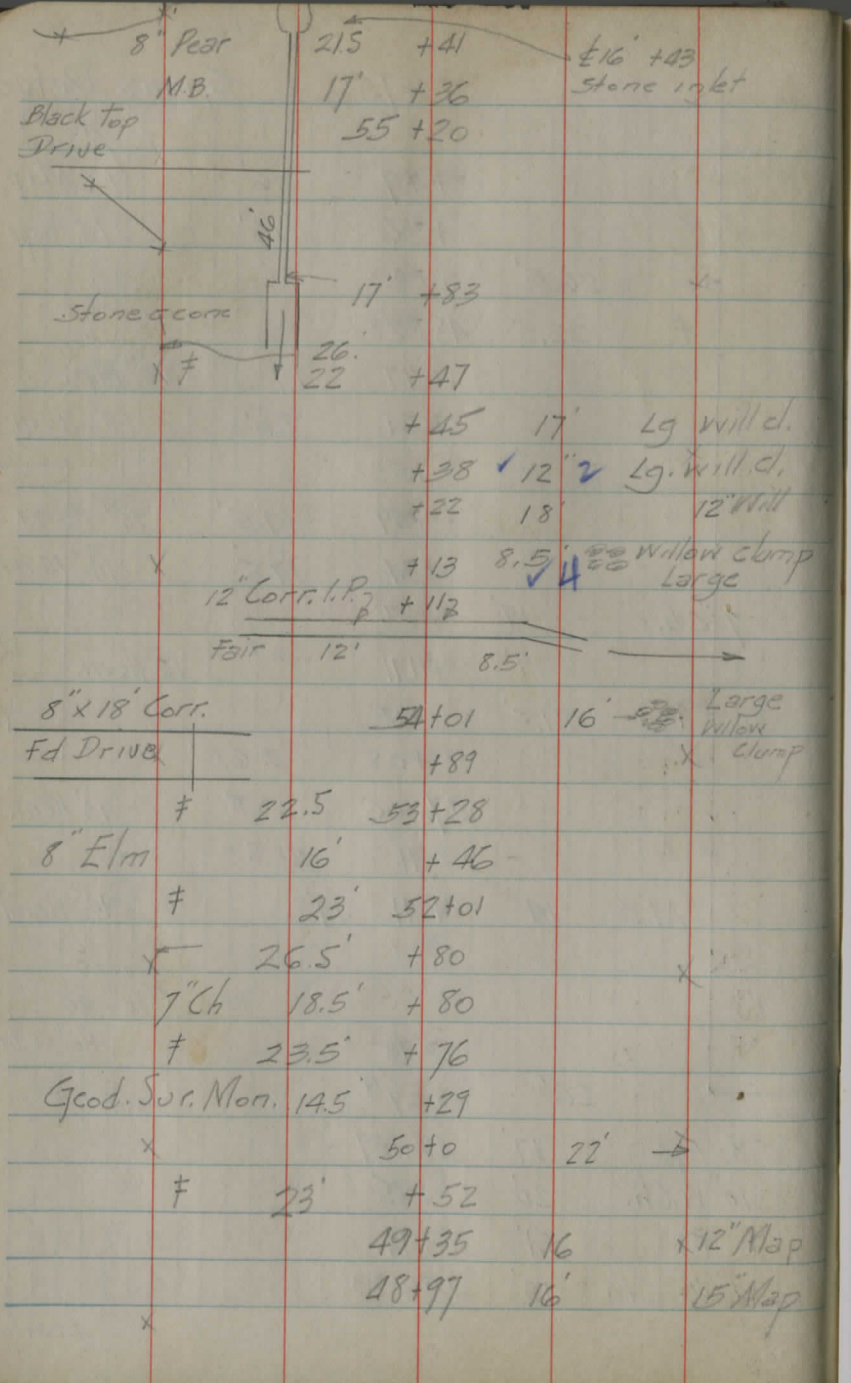
		+27	16.5	14" Map
		+26		
8" Elm	23	+17		
#	16.5	30+04	21'	
8" Elm	22'	+97		House
		+77	±6.5'	
		+60	16'	15" Map
8" Elm	22'	+45		
7" Elm	22'	+29		
		29+27	16.5'	13" Map
		+95	16'	14" Map
				4" drain
F	14	+81	8.5'	(4" Evergrns ±4' back of fence)
10" Elm	16'	+72		
		+50	22	
		28+47	18	13" Pear
		+83	14.5'	18" Elm
#	10'	27+61		
8" Corr. Not too good		+78	2' 20'	
		+34	23'	#
		+15		Drive
10" Ash	19'	26+04		
10" Elm	21'	24+80		


12" Corr
12" VSP
14'
12.5 +99
26" Map
± 31'
+94
PI
Drive
+60
40" Map
± 32'
+54
13.5
18" Map
+42
MB
12'
+38
12" Corr
Stone Hdwl
11'
+27
10" Elm
12
32+24
6" Elm
12'
+89
+80
16'
15" Map
7" Elm
11.5
+67
± 80'
+50
≠
+50
+42
21
+42
16'
16" Map
2" Evergn
21'
+11
11" Elm
23'
31+08
9" Map
19.5'
+93
+76
17'
13" Map
MB
11'
+67
10" Elm
12'
+67
30+40
Drive

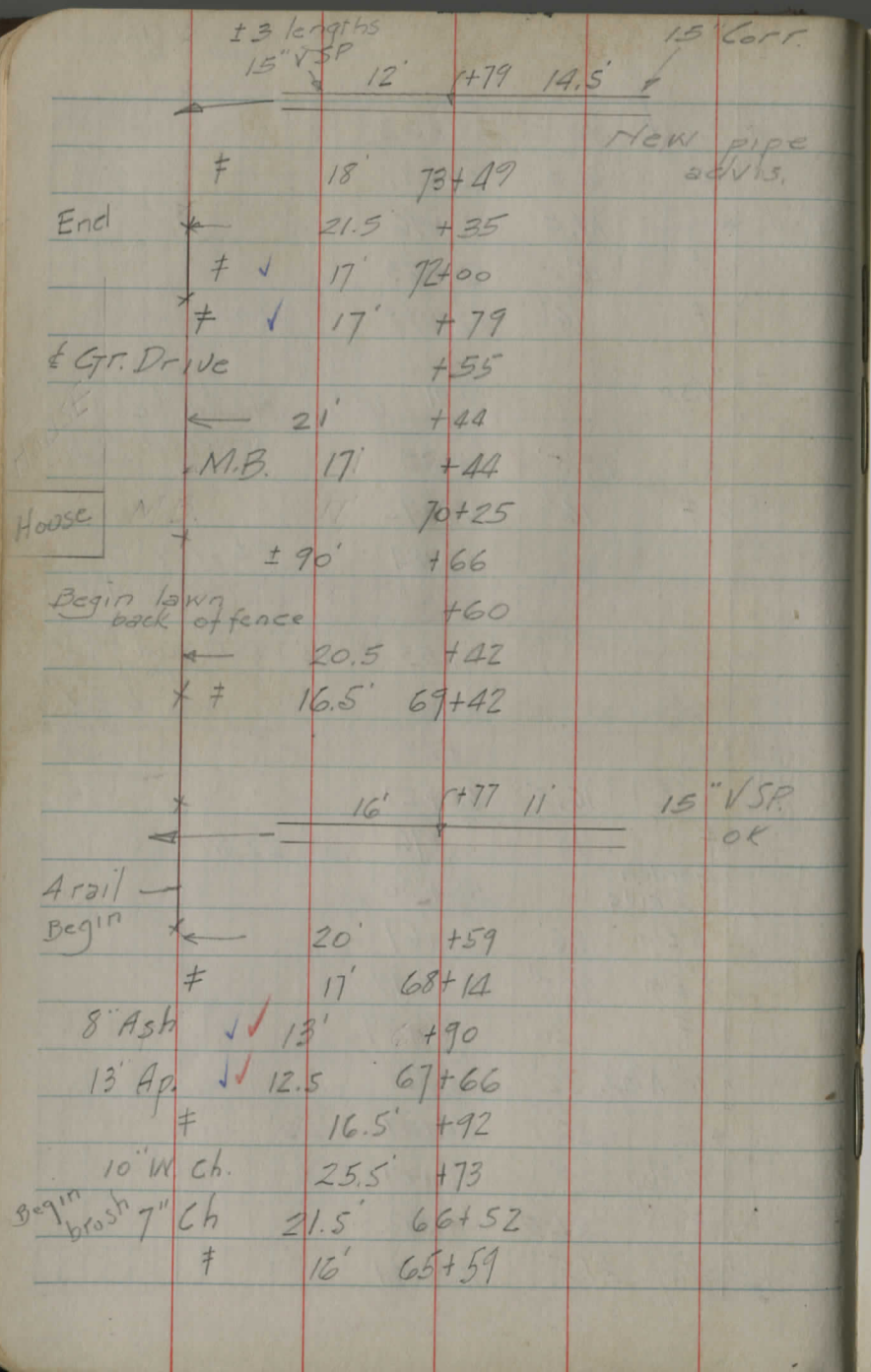

10" Ap
13.5
+98
≠
23.5
+83
39+0
21.5
10" W.Ch.
15.5
+85
8" W.Ch
21.5
+61
≠
23.5
+58
7" Elm
14
38+49
8" W.Ch.
23.5
+93
8" Ap.
15.5'
+78
12.5'
+55
14.5
12" Corr. OK
≠
25'
37+39
12" W.Ch.
23.5'
+86
8" W.Ch
16'
+72
8" W.Ch.
23'
+51
12" Elm
21'
+44
10" W.Ch
19'
36+26
7" Elm
23.5'
+24
10" Elm
22.5'
35+12
21.5
15" Map
29'
+56
15" Map
29'
+26
16" Map
29'
34+03
16" Map
29'
+74
10" Elm
23'
+69
8" "
19'
+49
12" x 16 Corr
13'
33+24
Begin brush
121'

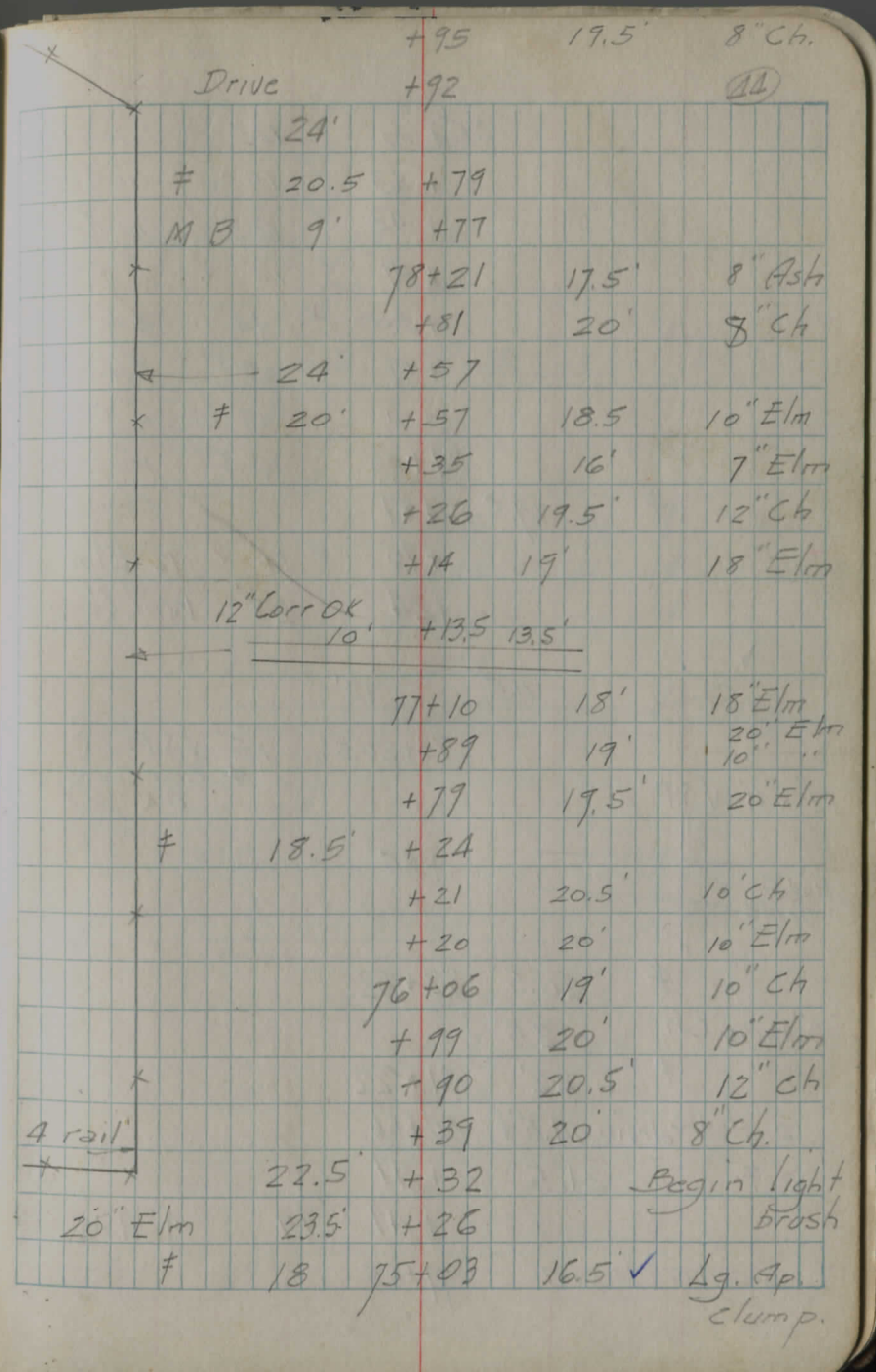

+93 16' 14" Map
≠ 21' +63
+58 10.5' barn drive
10'x20' corr
44+31
15" V.S.P. O.K.
14'
+88
15.5'
8" W Ch 20 +64
≠ 21 +49
9" Elm 14.5' ✓✓ +46
150 12
43+31 15'
Elm Clump
15" Ap
+95 24'
6" Ap. ✓✓ 13' +87
6" Elm ✓✓ 11' +85
8" W Ch. 21' +60
Elm clump 12' ✓✓ +58
8" Elm 9' ✓✓ +58
≠ 22.5' 42+21
7" W.Ch. 19' +47
7" W.Ch 21.5' +26
≠ 23' 41+0
10" W-Ch 22' +88
10" Elm 16' 40+04
Light
House


42
+75 Ginns Drive
+49 16' 18" Map
+36 16' +18" Map
26.5' +28
≠ 22.5 48+28
+77 19' 12" Ap.
+61 20' 18" Hem
+53
+49 19.5' 16" Hem
+34 19.5' 14" Hem
7" Ch. 19' +27
+17 23? 16" Hem.
≠ 21.5' +15
+08 ±65'
47+06 23.5 13" Hem.
+91 23.5
M.B 14 +91 19' 14" Heml.
4 Rail
corr.
10"x20
House Drive
+78
26' +67.17
8" Ap 17' 46+39
10" W.Ch. 20' +85
≠ 21' +79
14" W.Ch. 18' 45+33
House
4 rail



10" Ch. 10.5' +62
16.5' 64 +42
End 19.5' +96
16' 63 +63
16' 62 +98
8" V.S.P. +91 15.5' should be lowered this end
17.5' ? +72
16' 61 +72
+84 ℄ N "Y" Dines
+53 12' Geod. Sur mon.
℄ S "Y" Dines
+28
16.5 60 +27
18' +76 22.5'
Garden Drive
58 +30
8" Elm 26' +67
8" Elm 26.5' +49
20' 57 +29
10" Map 22' +52
26' 56 +07 22'
12" Map 22' 56 +07
21.5' +80
12" Map 21.5 55 +61
Shrubs right of fence


±3 lengths
15" VSP
12'
+79
14.5'
15 Corr.
New pipe advis.
End
Gr. Drive
House
Begin lawn back of fence
M.B.
Begin
4 rail
8" Ash
13' Ap.
10" W. Ch.
Begin brush
7" Ch
15" VSP OK


Drive
(11)
24'
M B
12" Corr OK
10'
+13.5
13.5'
4 rail
20" Elm
Begin light brush
Lg. Ap. clump.

85+00 ✓ 12.5' ✓ 10" Ch

+83 ✓ 15.5' ✓ 10" Ch

+48 ✓ 12.5' ✓ 10" Ap

+37 ✓ 12' ✓ 11" Ch

+30 ✓ 14' 8" Ch

+19 15.5' 8" Ch

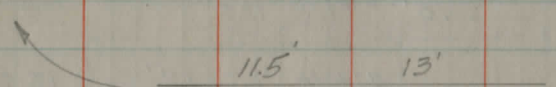
+11 17' 10" Ch.

84+05 15.5' 10" Elm

≠ 19.5 +87

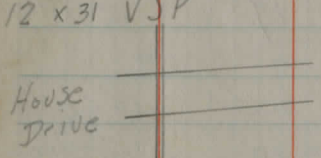
+70 ✓ 14' ✓ 12" Elm

+24 28' Will. Clump



83+20.5' 15" VSP & Corr. OK

12" x 31' VSP



+85

≠ 20.5' 82+52

3" tome Ch 25'

≠ 22' 81+22

3" House drain 14.5' ✓ 80+86

≠ 21.5' +77

+49 19 9" Ash

Begin lawn 79+05

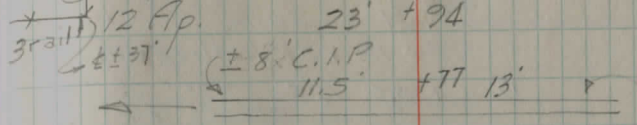
Light brush

14" Ap. 23 +89

12" Ap 23' +36

≠ 17.5' 90+06

Beg. thorn hedge 23' +94



+53 16' ? 10" Elm

+34 ✓ 14' ✓ 7" Elm

89+26 ✓ 15.5' ✓ 12" Ch

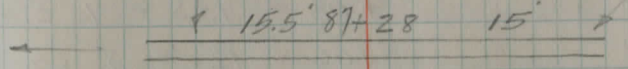
≠ ✓ 18.5' +84

88+62 17.5' ✓ ≠ guy

≠ 18 +58

Will. Clump 19' +54

18" Corr. poor ± 2 lengths



Will. clump 25' +90

+58 14.5' 12" Elm ?

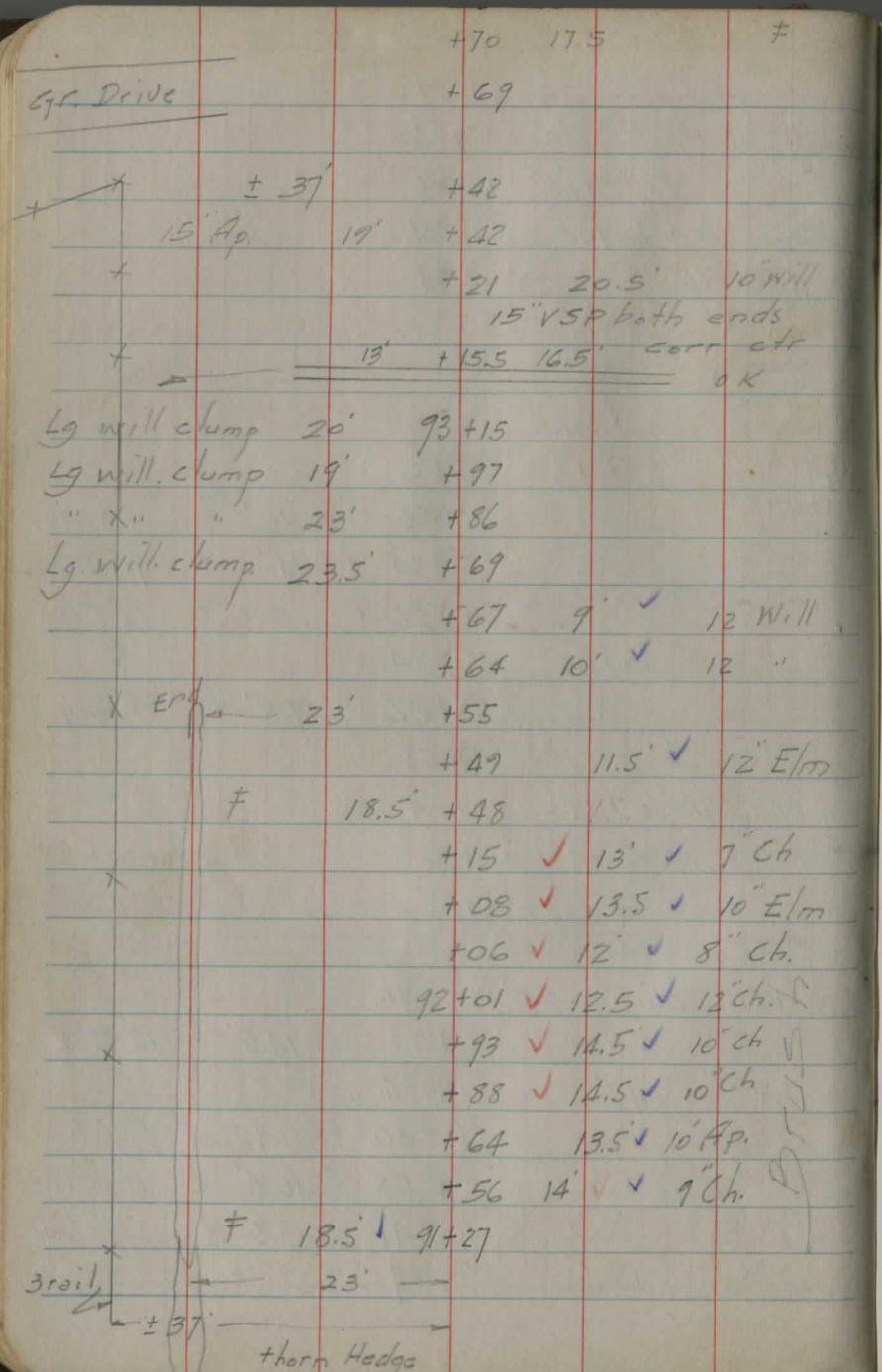
≠ 18' +34

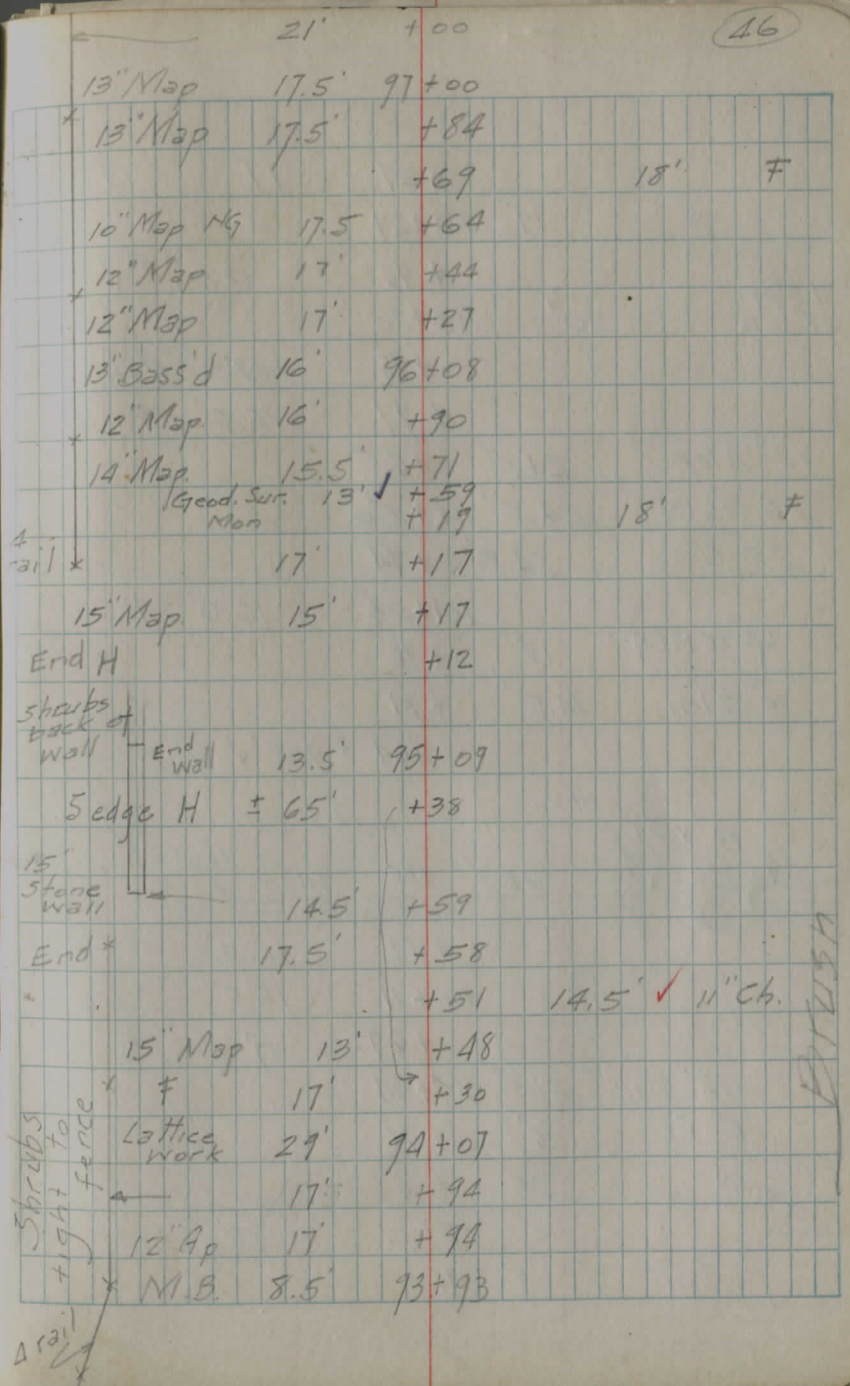
86+20 ✓ 14.5' ✓ 9" Ch

+58 ✓ 16.5' ✓ 11" Ch

+41 ✓ 13.5' ✓ 12" Elm

≠ 18.5 85+09


Gr. Drive
± 37'
15" Ap.
19'
Lg will clump
20'
Lg will. clump
19'
" X "
23'
Lg will. clump
23.5'
End
23'
F
18.5'
F
18.5'
91+27
3 rail
23'
± 37'
thorn Hedge
+70
17.5
F
+69
+42
+42
+21
20.5'
10" Will
15" V SP both ends
13'
+15.5
16.5'
corr. etr
ok
93+15
+97
+86
+69
+67
9'
12 Will
+64
10'
12 "
+55
+49
11.5'
12" Elm
+48
+15
13'
7" Ch
+08
13.5
10" Elm
+06
12'
8" Ch.
92+01
12.5
12" Ch.
+93
14.5
10" Ch
+88
14.5
10" Ch
+64
13.5
10" Ap.
+56
14'
9" Ch.


21'
+00
13" Map
17.5'
97+00
13" Map
17.5'
+84
+69
18'
F
10" Map MG
17.5
+64
12" Map
17'
+44
12" Map
17'
+27
13" Bass'd
16'
96+08
12" Map
16'
+90
14" Map
15.5'
+71
Geod. Surv. Mon
13'
+59
+19
18'
F
rail
17'
+17
15" Map
15'
+17
End H
+12
shrubs back of wall
End Wall
13.5'
95+09
5 edge H
± 65'
+38
15" stone wall
14.5'
+59
End
17.5'
+58
+51
14.5'
11" Ch.
15" Map
13'
+48
F
17'
+30
Lattice work
29'
94+07
17'
+94
12" Ap
17'
+94
W.B.
8.5'
93+93
Shrubs right to fence
rail

+29 17' ≠

19' 101+27

+93 12.5' stop

9 Map
22" to 12"

20' 103+20

+98 17.5' Ash Cl.

+77 16.5' ≠

12" Map. 21.5' +65

26" Ash 24.5' 102+50

28" Ch. 24.5' +94

101+23 16.5' ≠

35 MPH 13' +96

10" Elm 14.5' +74

+64 9.5' 7" Elm

M.H. Looks OK

18" V.S.P. 12" V.S.P.

22.5' +55 14'

+44 10.5' stop

100+11 16.5' 28" Elm

+69 17' ≠

Beg. Brush

12" Map. 21.5' 99+34

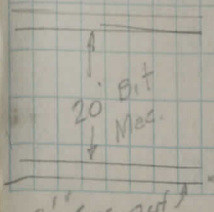
6" Ap. 26' +96

End fence 25' +32

98+19 17.5' ≠

7" Ash 19' 97+49

4 rail



±27'

No. Woodland ±15.5 Bit. Mac.

X Sections Co. Line

	+	HI		−
B.M.	0.95	1038.89		1037.94
T.P.	0.55	1026.66	12.78	1026.11
T.P.	0.60	1015.85	11.41	1015.25
B.M.	0.42	1008.65	7.62	1008.23
104+0				1004.2
103+0				997.4
T.P.	5.66	1002.17	12.14	996.51
103+0				
T.P.	0.16	996.67		996.51
102+0				993.0
101+0				991.7
100+55	Culvt			991.9
100+0				992.5

Road (N. Wood. South)

9+25 N. Woodland

Bent spike (& washer) SE side 1st Map. SW quadrant intersection N. Wood.

West ℄ East

2.0 4.6 5.3 4.5 — 4.9 4.4 2.5 2.0 2.4
16 11 9 — 11 13 16 20.5 30
30

4.0 4.6 4.8 5.7 12.0 11.3
30 25.5 23.5 19 8

996.9
5.3 6.2 5.3 2.9 2.3 3.1 4.0
℄ 8.5 12 13.5 16.5 20 23 30

+0.4 0.8 3.4 3.9 4.5 4.2 3.7 — 4.1 4.9 4.5 4.8 4.5 4.8
30 22.5 16.5 13.5 9.5 6.5 — 7.5 10.5 15 20 25 30

4.5 4.8 4.5 5.9 5.3 5.0 — 5.4 6.0 5.8 6.3 5.9 6.2
30 17 14 10.5 8 — 6.5 9 11 15 18.5 30
20.5

10.47 Bot. M.H. F.L. — 4.8 — 9.09 F.L. — 5.7 ± 100

4.0 4.3 5.2 4.4 4.2 4.5 4.2 4.5 4.7 5.7 5.4 1.6 1.8
25 21.5 18.5 16 12 9 — 5 9 10.5 12.5 25 30

	+	HI	−	
		996.67		
T.P.	5.27	999.45	2.49	994.18
99+0				994.4
T.P.	5.56	999.74		994.18
98+0				994.6
97+0				995.6
T.P.	6.73	1005.84	0.63	999.11
96+0				1000.3
T.P.	9.97	1009.08		999.11
95+25				1004.4
				1003.6
95+0				
T.P.	1.52	998.04	12.56	996.52
94+02	M.H.	9'	Filled	
94+0				995.2
		Drive		
93+15		Cut		992.6

1.6 1.7 6.4 5.4 5.1 5.3 5.8 6.5 1.3 0.4 1.0
30 20.5 13.5 11 5.5 8 10.5 16 20.5 30

56
30
7.6 6.6 6.5 6.7 6.3 5.5 5.1 5.6 6.2 5.6 5.6
24 20 16 14.5 12.5 10 8 10.5 12.5 30

4.8 4.0 4.3 5.6 4.7 4.1 4.8 5.4 4.8 4.2 3.8 3.5 3.8 3.7 3.5
30 21 14 11 9 E 9 10.5 12 14.5 18.5 21 22 25 30

5.0 4.2 4.3 4.8 6.4 6.0 5.5 6.2 6.0 2.4 1.8 1.6
30 22 17 13 9.5 7 9.5 11.5 16.5 18.5 30

2.9 2.0 2.1 2.8 3.9 5.4 4.7 5.3 4.5 1.5 1.3
30 20 17 13 9.5 7 11 12.5 16 30

4.2 3.0 5.4 2 4.8 6.1 5.5 6.1 5.5 2.3 2.2 2.7
15 to P 11 8 5.5 11 12.5 17 25 30
30 wall 13.5
1A

0.0 to 3 0.4 2.4 3.1 5 2.5 2.9 2.8 3.1 2.8 1.7 2.4 3.1
30 17.5 14.5 11 to P M H 7 5 12.5 14.5 17 25 30

1.5 3.2
60 30

10.4 9.1 5.4 8.3
45 FL FL

998.04

93+0				992.04	
BM.	7.73	999.03	6.74	991.30	
92+0				993.3	
+50				994.9	
91+0				993.3	
T.P.	5.46	995.95	8.54	990.49	
90+0				989.7	
89+77	Culvt ± 6Ac			989.5	
89+0				990.2	4.6 30
+65				991.3	
88+0				988.6	

W E

7.7 7.2 6.6 6.0 5.6 5.8 5.7 6.7 5.7 5.2 5.0
22.5 18 13 9.5 7 10 12.5 16 19.5 30

Spike S side 10" Willow (in clump)
Sta 92+86 26' Lt (West)

6.0 4.9 4.7 4.9 6.6 6.0 5.7 5.9 6.3 1.2 +0.7
30 23 20 15.5 12 9.5 3.5 6.5 13 18.5 30

3.6 2.7 2.3 3.2 4.9 4.1 4.5 +1.1 +1.8 +1.5
30 24.5 17.5 15 12.5 5.5 12.5 16 30

3.8 2.9 4.4 6.3 5.8 5.7 6.1 6.3 2.3 1.8 2.4 2.6
30 18 14.5 11 7.5 4 6.5 13 17 25 30
25

10.0 8.0 6.9 6.5 6.3 6.7 6.7 6.9
30 14.5 10.5 7.5 7.5 18.5 30
13

12.2 10.16 6.5 8.9
50 FL FL

4.1 3.4 4.4 6.1 6.7 6.1 5.8 6.5 5.8 2.5 1.8 2.2
25.5 22.5 18.5 15 12 8 9 11 15.5 18.5 30

1.8 1.4 1.6 4.1 4.3 5.6 5.2 4.7 5.0 5.2 0.7 +0.1 0.5
26.5 21.5 18.5 14.5 13 12 9 5.5 8 16 19 30

5.9 5.8 5.4 5.8 7.7 7.9 7.6 7.4 7.5 7.8 7.4 6.4 6.0 6.6
30 25 20 17 14 11 8.5 4.5 10 13.5 16.5 20 30

		995.25			
87+28	Cult		7Ac	988.1	
87+0				987.8 ± 13.5 30	11.5 19.5
T.P.	10.45	998.73	7.67	988.28	
86+0				990.5	
+40				994.0	
85+0				992.8	
T.P.	5.54	995.99	8.28	990.45	
84+0				990.5	
+20		Cult	2Ac	990.4	
83+0				990.7	
82				991.9	

12.3 7.9 11.7
FL FL

10.7 9.4 8.1 8.4 8.0 7.7 8.2 8.4 8.3 8.8 8.6 9.1 8.4 8.2
16.5 14.5 11.5 10 7 ℄ 7 9 11 13 15.5 19.5 25 30

7.4 6.4 7.2 8.2 8.9 8.3 8.2 8.7 8.1 6.3 4.4 3.7 3.7
30 21.5 17 14 12 7 7.5 10 13.5 17.5 25 30

3.2 2.7 2.9 5.0 4.8 5.8 4.7 5.6 4.6 2.0 1.6 1.1
30 24 18 15 13 12 7.5 11.5 16 21 30

4.4 4.0 4.4 5.9 6.7 6.4 5.9 6.5 6.9 6.0 3.7 3.4 3.0 3.0
30 22.5 17 14.5 11.5 8.5 6.5 9 12 15.5 19 25 30

6.6 6.2 6.4 6.0 6.2 5.8 5.5 5.9 6.1 5.5 4.0 3.9 4.0
30 24 18 13.5 10.5 7.5 10.5 12 14.5 20.5 25 30
7.5

9.2 8.8 5.6 8.3
50 FL FL

7.6 7.5 7.2 6.3 7.9 5.9 5.3 5.4 5.5 5.2 5.1 5.0
26.5 22 18 14.5 11 12 8 6 15.5 18.5 25 30
10

5.1 drive
50

10.0 0.6 1.8 4.5 4.3 5.0 4.5 4.1 4.5 4.8 3.6 4.6 3.9 3.1
30 21 16.5 12 10 8.5 5 6 9.5 13 15.5 19 30

		995.99		
T.P.	11.20	1005.91	1.28	994.71
81+0				995.4
80+0				999.8
T.P.	7.07	1011.06	1.92	1003.99
79+10				1005.4
+80				
				1006.8
78+0				1005.5
77+13.5	cult		3/4 Ac	1005.4
77+0				1005.2
T.P.	6.75	1012.03	5.78	1005.28
76+0				1005.7
+35				1006.5

57

3.3 5.0 6.2 8.7 12.0 11.1 10.5 10.7 10.9 11.3 9.8 10.4 10.7
30 21.5 17 12.5 8 5.5 9 12.5 15.5 19 22 30
10.5

1.4 2.2 4.9 5.7 7.0 6.6 6.1 6.6 6.9 6.6 6.8 5.7 6.1 6.2
25 19 11 9 7.5 5.5 8.5 10.5 12 13 15.5 19 30
30

4.1 3.1 3.4 5.0 5.8 5.7 6.0 3.6 3.8
30 18 12.5 8 4 11.5 17 30

46 drive
60

4.3

7.1 6.3 5.9 5.3 6.0 5.6 5.9 6.3 4.8 3.9 3.3 2.4
27 16 12 9 6.5 9 12 15 18.5 21.5 30
23 25

8.4 5.7 7.25
FL FL

8.8 7.8 7.3 7.0 6.3 5.9 6.2 6.8 5.8 5.4 5.1
30 21 15.5 9.5 6 11 14 18 25 30

7.3 6.5 6.6 6.4 5.9 6.9 6.3 6.6 6.9 4.3 3.9 3.4 3.3
30 22 14 11.5 9 6 8.5 11.5 16.5 19.5 25 30
19.5

5.8 4.9 4.6 6.2 5.8 5.5 5.8 6.2 3.1 2.4
30 13 9 6 3 8.5 12 17.5 30
22.5

10.12.03 ✓

BM.			3.84	1008.19 ✓
75+0				1004.6
74				1001.8
T.P.	8.39	1010.32 ✓	10.10	1001.93 ✓
73+79		calvt 1½ Ac		1001.8
73				1002.2
72				1004.4
T.P.	7.12	1016.97 ✓	0.47	1009.85 ✓
71				1009.6
+55				1011.2
70				1008.9
T.P.	8.99	1015.60 ✓	10.36	1006.61
67				1005.9

13.9
23

53

Spike SE root 20" Elm 75+26 Lt 24'

6.4 5.5 5.6 5.8 7.2 8.1 7.4 7.4 7.8 7.2 5.7 5.0 4.6 3.5
30 18.5 16.5 10.5 7 5.5 8 11.5 13.5 15 17 19 30

12.6 13.0 12.3 12.0 11.4 10.5 10.6 10.2 10.1 10.6 10.1 11.0 10.3
30 25 16 13.5 9 6.5 5 9 13.5 17.5 21 30
17.5
23

Plenty Fall 11.4 8.5 10.4
F.L. FL

11.1 10.2 10.1 9.1 8.2 8.4 8.1 8.2 8.3 8.9 7.9 8.2 7.8 7.3 6.9
25 20 15 10 7.5 6.5 7 10.5 12.5 15.5 17 18.5 25 30
22

3.4 3.7 4.2 5.4 6.7 6.3 5.9 6.1 6.3 5.7 6.1 5.1 5.3 4.9 4.6
21
30 18 14.5 11 9 5.5 ℄ 6.5 8.5 11.5 13.5 18.5 21 25 30

4.9 6.7 7.0 7.6 – 7.4 7.5 7.7 5.1 4.4 3.8 4.0
21 15.5 13 9.5 8 2.5 5.5 10 18.5 25 30
30

drive 5.7 4.6 5.1 5.2 5.8 6.1 3.3 2.4 2.1 1.9
60 30 14.5 9 4 9 16 23.5 30

7.7 7.8 8.0 8.7 9.2 – 9.0 7.2 7.6 7.4 5.8 5.3 5.6
30 25 20.5 15 12.5 9.5 5.5 9 14.5 20 25 30

12.8 12.0 10.5 10.1 9.7 9.4 9.5 9.7 9.9 10.4 10.5 10.1 8.7 8.1 8.3
19 14.5 12 10 6.5 ℄ 4 7.5 10.5 11.5 14 17 20.5 25 30

		1015.60		
68+77		culvert	3/4 Ac	1006.2
68+0				1006.9
67				1010.5
66				1010.8
65				1012.6
T.P.	7.29	1020.89 ✓	2.00	1013.60
64				1015.9
63				1015.2
62				1014.6
61+91		Culvt		1014.7
61				1014.9
BM			5.13	1015.76 ✓

Plenty fall 13.1 9.4 12.1

FL FL

7.6 7.0 7.6 9.1 8.5 9.2 8.7 9.0 9.2 8.1 7.6
30 20 14 10.5 9 5 6 9 18 30
13

5.7 5.3 4.8 4.5 4.6 5.7 5.1 5.6 5.8 4.0 3.7 3.2
16.5 23 18 13.5 12 8.5 6 9 13.5 19.5 30

7.7 7.8 6.8 6.7 5.8 5.2 5.4 4.8 5.1 5.3 4.8 5.2 4.6
26 23.5 20.5 16 12.5 10 7.5 7 10 13 17 30

1.7 1.6 2.0 3.3 3.8 3.4 3.0 3.3 3.7 3.2 1.9 1.8 1.2 0.9
20 16 11.5 9.5 8 4.5 7 10.5 12.5 15 19.5 25 30
30

5.9 6.0 5.6 5.4 5.6 5.0 5.2 5.8 4.9 5.0 4.5 4.3
31 24.5 19 8.5 6.5 8 12.5 15.5 18 25 30
13

5.2 5.1 5.8 6.5 6.2 5.7 5.7 6.4 5.3 5.0 4.8
16.5 12 9 7.5 4 7 11.5 18.5 25 30
30 14

8.7 8.3 8.4 7.9 7.5 7.3 6.7 6.3 6.4 6.7 6.6 6.9 7.4 7.1 7.0 6.8
30 24 21 18 11.5 9 6 6 10 13 16.5 17.5 20 25 30

8.2 6.2 7.6
top Tile FL
I 10"

6.0 5.9 6.1 6.2 6.4 6.2 6.0 6.2 5.6 6.0 6.2 6.0 5.6
30 19 14.5 11 8.5 6 8 11 13 16.5 21 30

Geodetic Survey Mon. inter. Pines
on Pines & Survey

60+0				1017.1
T.P.	3.62	1021.32	3.19	1017.70
59				1017.6
58				1016.4
57				1015.4
56				1011.6
T.P.	2.37	1012.96	10.73	1010.59
inlet drive pipe			4.9	1008.1
outlet " "			5.9	1007.1
Drive			3.3 36	1009.7
55				1008.7
54+11	Culvt	½ Ac		1007.8
T.P.	2.77	1013.36		1010.59
54				1007.6
53				1008.6
52				1009.1

3.1 3.5 4.4 4.3 3.8 4.3 3.9 3.2 2.5 2.6
30 20.5 12.5 10.5 7.5 5 7 9 17 25 30
12

5.6 4.9 4.6 4.3 4.5 4.3 3.7 3.7 4.2 3.6 3.3 3.5
30 20.5 16.5 12 9.5 6.5 5.5 9 10.5 16 22 30

4.7 4.5 4.6 5.2 5.5 5.3 4.9 5.2 5.7 5.2 4.7 4.2 3.9
30 21.5 16.5 12 9.5 6.5 6.5 10 11.5 15 20 25 30

6.3 6.5 6.2 6.4 6.2 5.9 6.3 6.9 6.5 6.6 7.0 6.9
24 18 13.5 10.5 8 6 9.5 11 14 19.5 25 30
30

6.3 6.8 7.1 7.8 10.5 10.1 9.7 9.9 10.3 8.4 6.5 6.2 6.5 6.4
30 24.5 22.5 19.5 14.5 10 4.5 7.5 11 13.5 16 20.5 25 30

4.2 4.7 4.5 4.3 4.8 4.1 4.0 2.5 1.9 1.8
30 18.5 11 6 8 9.5 13 25 30

6.9 5.2 7.1 Plenty fall
FL F.L.

5.5 5.7 5.5 6.7 6.0 5.8 5.9 6.6 7.7 8.6 8.8
30 22.5 18 15.5 11.5 6 9.5 16.5 25 30

1.3 2.0 5.6 5.2 4.8 5.1 2.3 3.3 3.4 3.7
25 14.5 10 8.5 7.5 12 20 25 30
30

3.5 4.0 4.3 4.7 4.3 4.7 5.2 4.7 6.6 7.2 7.0
25.5 21.5 12 10 6 9 10.5 25 27 30
30

		1013.36		
51				1009.4
T.P.	4.44	1014.29	3.51	1009.85
50				1010.1
BM.			4.04	1010.25
49				1010.2
48				1008.1
47				1005.0
T.P.	1.97	1003.11	13.15	1001.14
46				997.8
45				993.4
T.P.	2.72	995.81	10.02	993.09
44				991.0
				991.0

2.6 3.4 4.8 4.0 4.4 4.0 5.0 5.3 5.7
22 13 10.5 7.5 10.5 25 25 30
30

3.7 4.5 4.9 4.2 4.9 5.0 6.4 6.8 7.0
33 13.5 11 7.5 11.5 25 26 30
30

Spike W root 12" Maple 49+35 16' Rt

3.1 2.8 3.9 4.7 4.7 4.1 4.7 4.0 4.2 4.9 5.1
30 25 13 10.5 9 7 10 20 24 30

drive 4.8 5.8
24 40

4.3 4.9 5.0 6.6 6.3 6.2 6.7 5.2 6.4
25.5 20.5 16 12 8.5 6 10.5 25
30 30

6.0 6.7 10.0 9.5 9.3 9.9 7.9 7.4
26.5 19.5 13 7 5.5 11.5 25
30 30

drive 10.3 9.6
8 30

1.6 1.2 1.6 5.8 – 5.3 5.6 6.3 1.8 1.2 1.1
30 23.5 20 13 9 4 6.5 14 18.5 25
30

6.9 6.1 6.4 9.8 10.6 9.8 9.7 10.4 7.9 7.6 8.4 8.8 9.1
30 23 21 14.5 12 8.5 6 7.5 10 12 25 30

drive 5.8 3.7
9 30

4.1 4.5 6.0 5.2 – 4.8 – 5.2 6.7 7.9
22.5 14.5 12.5 11.5 10 7.5 13 17 25
30 13.5 30

7.3 4.8 8.9 Plenty fall
FL FL

		995.81		
43				991.2
T.P.	7.27	1000.16	2.92	992.89
42				993.0
+20 ℄			4.3	995.9
41				995.3
40				990.4
T.P.	3.27	992.34	11.09	989.07
39				988.7
38				987.5
+55 Culvt		1 Ac		987.1
37				987.6
36				988.1
35				989.5
T.P.	9.74	999.96	2.12	990.22
34				992.8

0.8 2.3 5.4 4.9 5.2 4.6 5.0 5.7 6.9 7.4
26.5 17.5 10.5 9.5 8 7.5 16 25 30
30

3.2 3.5 4.5 5.2 7.8 7.2 7.7 6.7 6.9
30 24.5 19.5 12 7 10 13 25 30

0.4 0.0 1.1 5.5 4.9 5.6 4.2 4.9
30 25 18 8.5 9 12.5 25 30

8.0 9.8 9.9 10.8 9.8 10.5 9.4 9.7 10.1 9.7
21.5 15.5 13 10.5 8 12 20 25 30
30

1.9 1.5 2.4 3.7 4.6 3.6 4.5 4.3 6.2
30 25.5 22 12 8 9 11 25 30
15

3.5 3.2 3.5 4.0 5.0 5.5 4.8 5.3 5.6 6.8 6.5
30 25 19.5 17 12 9 7.5 11.5 25 30

7.0 5.2 8.8 Plenty fall
FL FL

3.8 5.2 5.7 5.2 5.0 4.7 5.1 5.6 5.7 5.2 5.1 5.5
27.5 16 14.5 13.5 8 9 10.5 13 14 24 25 30

2.8 3.3 4.1 5.0 4.5 4.7 4.2 4.8 6.2 7.6
30 24 16.5 15 13.5 8.5 9 12 25 30

0.4 1.6 3.2 3.8 2.8 3.8 2.8 3.8
27 18 12.5 12 10 12.5 25 30

1.9 2.2 2.5 8.6 8.0 7.4 7.2 7.8 4.1 4.0
30 26 22 12.5 12 10 8 13.5 25 30

3.7 6.5
FL FL outlets

		999.96		
33				995.6
BM.			2.87	997.09
32				997.5
32+60	drive			
T.P.	4.61	1002.38	2.19	997.77
31+30				998.7
31+0				997.5
	drive			
30				
T.P.	0.18	989.86	12.70	989.68
30				988.9
29				981.8
T.P.	1.78	981.09	10.55	979.31
28				978.3
27				975.7
26+78	Culvt			976.0

3.6 4.5 4.8 6.2 4.9 4.4 5.1 4.7 4.5 5.2 6.6 8.0
30 24.5 14.5 12 10 9 10 17 21 25 30

Spike NE root 26" Maple 32+94 30' Rt
+0.2 1.5 3.5 2.5 3.5 3.0 4.6 5.0
30 14 10 9.5 11 25 30

1.5 3.3
50 15

1.4 3.1 4.1 3.7 4.2 2.6 3.8
30 10 8 8 11 25 30

1.8 1.6 1.9 5.4 4.9 5.6 2.7 3.5
30 25 18.5 8.5 7.5 11.5 20.5 30

+ 5.8 6.8 8.2 9.1
50 33 12

994.0 992.8 993.4 993.8 994.2
8.4 7.6 9.0 8.6 8.2
25 16 12.5 21 30
30

1.5 1.0 1.5
10 5.5

3.8 4.4 4.7 8.7 8.1 8.7 4.7 2.8
25 21 17.5 10.5 6.5 11.5 18 30
35

3.4 3.6 3.8 3.4 3.1 2.8 3.2 1.9 1.3 0.5
40 25 17.5 10.5 7.5 9.5 21 22 30

2.3 5.1 5.4 5.6 5.4 4.3 5.4 5.9 6.0 5.7 5.9
42 25 10 5 13 15.5 17.5 18.5 21 24.5

6.5 5.1 7.2 Lots Fall

		981.07		
26				976.9
T.P.	11.03	991.37	0.75	980.34
25				983.9
+50				986.6
24				
				984.5
T.P.	2.46	984.62	9.21	982.16
23				980.8
22+04	Culv't 2.5 Ac			980.0
22				979.9
T.P.	5.96	986.91	3.67	980.95
21				982.1
+70				982.4
20				976.8
T.P.	0.66	974.68	12.89	974.02
19				968.7

+0.8 0.3 0.6 4.1 4.3 4.9 4.2 4.1 4.7 5.4
40 25 21 12 8 7 11 13.5 23

1.6 2.0 3.1 8.0 7.5 8.0 4.5 4.6
30 25 15.5 7.5 9 16 20.5
40 30

0.6 0.2 0.6 1.9 4.0 5.4 4.8 4.9 5.4 3.8 3.9 4.2
28 25 23 12 8 6 7 10 13.5 20.5 30
35

2.3 2.1 3.1 7.4 6.9 7.3 4.4
25 20.5 12 6 10.5 16
30 21.5
30

2.2 3.4 3.8 4.3 3.8 4.2 3.7 4.0
17.5 11.5 7.5 7 9.5 10 21
30 30

6.6 4.6 7.0 Plenty fall
FL FL

5.3 5.2 4.6 5.0 4.7 5.1 6.6 7.2
30 8.5 6.5 6 10 21 30
15

1.8 1.2 1.5 1.9 4.8 5.6 4.8 5.4 4.2 3.2
25 22 17.5 13 8 7 8.5 10 20.5
30 30

1.2 1.4 4.4 5.4 4.5 5.0 2.5
15.5 12.5 8 7.5 8 13
30 30

6.5 6.1 5.8 5.7 10.6 10.1 10.0 10.7 6.6
30 25 18.5 14.5 5.5 3 11 18
21 30

4.7 2.8 5.8 6.3 6.0 6.5 5.8 4.8 4.1
30 17 7 4 13 15 20 25

974.68

18+25	Culvt + 4.5 Ac			967.4
T.R	4.88	972.23	7.33	967.35
18				967.1
BM.	9.08	975.54	5.77	966.46
17				970.3
T.P.	11.47	986.68	0.33	975.21
16				977.9
+50				980.6
15				978.4
T.P.	4.14	980.44	10.38	976.30
14				975.5
13+78	Culvt .1 Ac			975.7
T.P.	9.26	987.67	2.03	978.41
13				978.1
12				983.5
T.P.	8.77	996.02	0.42	987.25
11				987.4
9+90				991.4

11.9 7.3 15.4 21.2

FL FL gd below FL

2.5 2.9 3.0 2.6 3.1 4.1 5.5 5.1 4.7 5.1 5.9 9.4 11.3
30 25 21 18 15.5 9 4 5 12.5 17.5 26.5 35

Spike SW root 8" Elm 17+88 20' Rt

0.0 0.4 0.5 2.4 5.6 5.2 5.0 5.2 5.6 2.1 1.6
30 25 15.5 9.5 3.5 4 9 11.5 17 25

4.7 5.0 4.6 9.3 8.8 8.7 8.8 8.4 6.1
40 25 12.5 5.5 4 11 12.5 17
8.5 23.5

1.2 2.2 6.0 6.6 6.1 5.3 5.6 4.8 4.9
50 14 5 3.5 6 15 18 25
25

1.4 2.2 2.5 8.2 9.0 8.3 8.4 5.6 5.9
50 25 19 9 8 8.5 14 20.5

5.3 6.2 6.0 6.6 5.2 4.9 5.2 5.7 6.5 10.6 13.1
35 25 18.5 15 12 5 8.5 13.5 22.5 27.5

8.4 4.7 13.1 17.7

FL FL gd under FL

4.7 4.5 8.3 10.3 10.1 9.6 10.0 9.8 6.4 6.9
30 20.5 13 10 6.5 7.5 10 16 30
25 25

0.1 +0.9 1.7 5.3 4.2 4.6 4.4 3.3 4.1 4.8 5.2
30 25 12 6.5 8 9.5 11.5 16 21.5 30

3.3 2.8 4.3 9.4 9.0 8.6 9.1 6.2 6.5 7.5 7.9
30 25 13.5 6.5 5 7.5 12 18 25 30

2.4 2.0 2.4 3.6 4.6 5.1 4.6 4.7 4.4 4.9 5.3 6.1
30 25.5 23.5 17 12.5 11 4 6 11 17 30

		996.02		
BM.			5.13	990.89
drive				
T.P.	6.71	1000.73	2.00	994.02
9				993.6
T.P.	4.13	998.15		994.02
8				993.6
7+40		cult 99.4% ord H_2O		993.4
7				993.5
T.P.	5.13	1000.01	3.27	994.88
6				995.2
T.P	2.03	996.91		994.88
5				992.1
4+19.5		culvert		991.9
T.P.				
4				992.1
T.P	10.17	1002.73	4.35	992.56
3				994.4
2				998.4
+50				998.5

Spike Hroot 14" Maple 10+57 Rt 15'

47
34

3.2 2.9 3.6 4.0 6.3 7.2 7.1 7.2 4.7 4.2 4.9 5.4
30 25 21.5 16.5 12 10.5 4.5 7.5 14.5 19.5 30

0.9 2.7 4.3 4.8 5.4 4.6 5.1 5.9 ± 8.9
24 15.5 12 10.5 9 7 14 30
30

6.2 4.8 7.4 Plenty fall
FL FL

1.0 1.3 2.6 3.5 4.7 4.6 5.4 4.7 5.4 5.2 5.9 7.4 8.0
30 25 20 14.5 11.5 10 8 8 9.5 13 20 30

2.0 2.7 3.2 4.3 5.4 4.8 5.7 5.4 5.7 9.7
25 19 13.5 9.5 8 7.5 9.5 15 30
30

+0.4 0.0 1.2 2.1 4.2 5.4 4.8 5.6 6.6 7.8 10.3
30 25 20 14.5 9 6 9 11.5 17 25

6.8 5.0 7.4 Plenty fall
FL FL

2.4 3.4 4.2 4.4 5.1 4.8 5.5 4.8 5.5 6.4 10.4
24 21 17 13 11 9.5 7 8.5 11 30
30

4.3 3.8 4.3 4.4 8.7 8.3 8.6 4.0 3.4 4.2
25 21.5 17 12.5 6.5 7 12 18 30
30

4.8 4.7 4.8 4.5 5.0 4.3 5.0 4.9 4.8 4.1 5.1
25 20 12 8 7 8 10 14.5 18 25
30 16.5 30

4.0 4.1 5.1 4.2 4.7 4.3 4.2 3.7 4.3
20 8.5 7.5 8 11 15.5 18.5 25
30 30

T.P	5.30	1002.73 / 1001.87	6.16	996.57
1+0				996.6
T.P.	1.12	997.69		996.571
BM.			3.89	993.80
0+0				992.0
0-100				989.0
0-200			℄ 10.2	987.5
0-300			℄ 11.3	986.4

\+ —

Sections taken on tangent at Co line

BM.	3.60	1011.83		1008.23
104+51 96				1006.3
10.5+0				1008.8
T.P.	3.58	1014.71	0.70	1011.13
+50				1010.9
106+0				1007.3

(4) Lt. Rt (5) 62

3.4 3.2 2.8 3.2 5.8 5.3 5.8 3.0 2.4
30 22 17.5 12 8.5 6 10 18
25 30

Horiz. Spike 5 root 36" Elm Lt 0+0

5.6 5.2 5.6 5.5 6.0 6.1 5.7 5.4 6.6 6.7 6.2 5.1 4.7
30 22 18 12 8 3 5 13 16 18.5 21 25.5
4.2 4.0
30.5 36

8.3 7.3 7.1 7.6 8.8 8.7 9.1 6.2 6.0 5.4 5.1
30 19 15.5 12 9.5 5.5 10 16 23 30

7.4 6.3 5.5 7.0
150 100 100

1.9 1.4 1.6 1.2 3.4 3.0 3.7 2.6 2.5 1.1 0.2 +0.1
27 24 18.5 13 9 8.5 11 14 18.5 25 30

4.4 4.5 3.6 3.5 4.2 3.8 4.4 3.9 3.6 2.7 1.9
30 25.5 21.5 14.5 10.5 7 8.5 10.5 15.5 30

5.5 6.5 7.8 7.6 7.4 7.1 7.7 4.6 4.3 2.5
26.5 18 13 10 4.5 6 13.5 20 30

	+	1014.71 ✓	−	
T.P.	0+30	1007.11 ✓	7.90	1006.81 ✓
		Drive		
✓ 107				1001.2
+40	cut	3 Ac		1000.9
TP	4.80	1005.91 ✓	6.00	1001.11 ✓
✓ 108				1001.8
T.P.	10.02	1015.41 ✓	0.52	1005.39 ✓
✓ 109				1005.2
T.P.	5.56	1020.15 ✓	0.82	1014.59 ✓
✓ 110				1013.0
T.P.	11.05	1025.64 ✓		1014.59 ✓
✓ 111				1119.6
✓ 111+50				1022.8

96 101.9

0.6 + 1.4

20 40

6.7 6.6 5.9 6.4 6.8 6.2 5.3 4.7 4.4

30 10 8 11 12 19 21 30

9.1 6.2 9.1

FL inlet FL inlet

7.90 inlet

outlet from M pipe 9.6

Bottom M.H 11.9

outlet from S ± 10.00

" from across rd 11.8

outlet ± 15"

4.9 4.9 4.1 4.7 4.8 5.2 5.2

30 7 11 16 20 30

Stk 109 ± 03 Lt ditch

5.0 5.1 5.8 8.2 11.2 10.7 10.2 10.6 11.0 10.6 7.1 7.2 7.3

30 21 17 13 8 4.5 7.5 9 11 18 25 30

2.7 2.8 3.2 8.1 7.7 7.1 7.5 8.0 6.2 4.3 3.9 4.5

30 21.5 15.5 8.5 6.5 6 9.5 12 18.5 22.5 25 30

2.8 3.2 3.9 5.0 6.5 6.0 6.3 6.8 4.2 4.1 4.5

30 20 14 10 8 5 10.5 14 20 25 30

3.0 2.8 3.0 3.5 2.8 3.6 2.0 1.8 1.9

26.5 18.5 11.5 9 9.5 13 20 30

	+	1025.64 HI	−	E
T.P.	4.64	1027.22	3.06	1022.58
112+0				1022.5
T.P.	1.21	1023.79		1022.58
113+0				1020.2
114+0				1018.3
115+0				1018.0
T.P.	1.28	1018.89	6.18	1017.61
116+0				1015.8
BM.			2.54	1016.35
culv+85				1013.6
117				1013.8
T.P.	12.98	1031.12	0.15	1018.74
118				1021.4
119				1030.1
T.P.	10.09	1041.42	0.39	1031.33
120				1034.4
121				1036.5

5.4 4.9 4.5 4.6 5.3 4.9 4.5 4.7 5.1 4.9 5.4 3.8 3.8 3.9
30 23 21 17.5 16 13 8 6 7.5 10.5 13.5 20 25 30

5.1 4.8 4.2 4.0 3.6 4.0 3.9 4.4 4.1 4.0 3.6
20.5 16.5 13.5 9 8.5 12 15 17.5 25 30
23

7.1 6.8 6.3 5.5 6.0 6.3 5.8 5.6 5.5
17 12 9 10.5 12.5 14 19.5 25
23 7.5 30
30

7.7 7.3 7.0 6.3 5.9 6.1 5.8 6.3 6.7 6.0 4.5 3.9 3.5 3.0
26 21 16 13.5 10.5 9 9.5 11.5 13.5 15.5 20.5 25 30

5.4 5.1 4.5 3.8 3.2 3.5 3.1 3.0 3.4 3.9 3.4 2.1 1.7 1.2
24 20.5 19 9.5 7.5 6 5 12.5 15 17 19.5 25 30

Spike W root 34" Maple Sta 116±4.5 Rt 26'
9.60 5.3 8.56
FL FL

8.4 8.2 5.5 5.2 5.1 5.3 7.6 7.8 7.9
24.5 18.5 13 9.5 9 13.5 17.5 25
30 30

9.7 10.0 11.6 10.7 11.1 10.6 10.3 10.5 11.3 11.1 11.2 11.5 12.2 11.6 11.8
25 19.5 16 13 12 8 8 10 14 17.5 21 23 25 30
30

2.0 1.9 1.6 1.5 2.9 2.2 1.6 1.7 1.7 2.0 2.2 1.4 1.4
30 26 20 15 12 10 5 9.5 13 14.5 17.5 25
30

8.5 7.9 7.5 8.1 7.8 7.0 7.3 7.7 5.9 5.3 5.1 4.6
30 23 17 15.5 12 10.5 14 16 20 25 30

6.1 5.8 5.4 6.0 5.4 4.9 5.1 5.4 3.8 3.5 3.2
26 21 15.5 13.5 8 7 16.5 20 25 30

		1041.42		
122		H.I.		1036.0
				1033.1
123				1033.3
T.P.	6.48	1040.16	7.74	1033.68
124				1035.4
T.P.	5.65	1039.33		1033.68
125				1034.5
	colut			1032.8
126				1032.7
	Drive			1034.1
127				1036.9
T.P.	13.12	1051.41	1.04	1038.29
128				1032.2
129				1035.8
+50				1036.6

All elev. 10 = high
from here 10 Add 10

5.9 5.4 6.7 5.8 6.0 5.4 5.6 5.7 6.0 4.2 4.0
30 19 15.5 11 10 6 10 13 17 25 30

12.1 8.3 10.7
F.L. F.L.

10.6 10.4 10.0 8.9 8.7 8.1 8.5 8.6 9.5 8.7 8.6 8.3 7.4
30 18.5 15 12 9 9.5 12.5 14.5 17 20 25 30

6.4 5.9 5.5 5.0 5.2 4.8 5.2 5.4 2.8 2.4
30 22.5 15.5 9.5 8.5 9.5 14 19 25 30

6.8 6.4 6.1 5.2 4.8 5.0 5.1 5.7 4.7 3.8 3.4
30 22 15.5 11.5 6.5 11.5 15 18 25 30

Ample fall 10.3 6.5 9.36
FL

10.3 10.0 9.6 9.3 7.0 6.6 6.8 7.2 8.7 8.8
30 24 20.5 14.5 10 7.5 13.5 17 25 30

6.6 5.2 5.2
±55 30

2.4 2.3 3.8 2.8 2.4 2.4 2.6 3.0 3.2 3.4 3.8
22.5 17 14 9 7 11 13.5 20.5 25 30
30

10.5 10.4 10.2 9.6 9.9 9.2 9.5 9.9 7.7 7.3 7.2
30 20 14 10.5 9 11.5 14 18 25 30
24.5

3.8 4.2 6.2 6.4 5.6 5.7 5.6 6.1 5.3 5.2
26.5 17.5 14.5 10 10 12 15 17 25 30
30

4.0 3.5 5.7 4.8 5.0 4.6 1.8 1.6
25 15.5 11.5 13 17.5 25 30

		1051.41			
130				1034.8	
	cult			1032.5	
131				1032.5	
T.P.	7.33	1051.87	6.87	1044.54	
132				1036.0	
+50			± 5.0		
133				1036.3	
134				1033.2	
T.P.	0.30	1040.06	12.11	1039.76	
135				1025.3	
BM.			3.48	1036.58	
	cult.			1023.9	
136				1023.7	
T.P.	7.56	1041.45	6.17	1033.89	stk 13610
137				1025.6	
+50				1026.8	

6.9 6.5 8.0 7.6 6.6 7.0 6.7 6.9 5.5 5.2 5.0
2.7 2.0 1.6 1.5 6 7.5 12.5 15.5 25 30

Plenty fall 12.3 8.9 11.0
F.L. F L

11.9 11.6 10.9 10.0 9.1 8.9 8.8 8.9 8.4 7.8
3.0 24.5 19 12 7.5 11 17.5 19 25 30

7.1 6.4 6.9 6.0 6.5 5.9 6.2 4.5 4.1 3.9
3.0 15 13 9 8 14 18.5 25 30

7.4 7.1 6.6 7.1 6.4 6.1 5.6 5.6 4.6 4.0 3.9
3.0 25 16.5 15 13 9 14 16.5 25 30

9.5 9.2 8.6 9.7 9.6 9.0 9.3 8.7 8.7 7.3 7.6 7.5
3.0 25 17.5 15 13 9 7.5 10 13.5 17 25 30

4.8 4.5 5.0 4.8 5.1 4.8 4.7 5.0 3.3 3.2
3.0 12.5 11 9 8 11 12.5 15.5 25 30

Spike W root twin Elm Sta. 135+12 Rt 25'
9.9 8.9 8.15 6.2 8.6
5.0 2.8 F L F L

8.9 8.3 6.5 7.3 6.9 6.4 6.6 6.8 5.3 5.3 4.5 4.1
3.0 2.3 11.5 9.5 7.5 6.5 9 12 15.5 25 30

5.1 5.1 5.3 6.9 5.9 6.2 6.4 4.5 4.9 4.1
2.7 3.0 2.0 14.5 10 4.5 7.5 10.5 16 25 30

3.5 3.6 3.9 5.6 4.7 4.9 3.5 3.8 3.5 3.7
3.0 2.1 13.5 9.5 8 10.5 13 25 30

		1041.45		
✓ 138				1024.2
T.P.	1.07	1029.63	12.89	1028.56
✓ 139				1013.7
T.P.	2.44	1018.91	13.16	1016.47
✓ 140				1004.4
T.P.	0.18	1016.65		1016.47
✓ 141				996.4
T.P.	0.62	1005.56	11.71	1004.94
✓ 142				990.9
✓ 143				988.1
✓ 144				986.2
T.P.	2.68	998.28	3.96	995.60
✓ 145				984.0
BM.			7.38	990.90
South end bridge			5.1	
N " "			5.3	
Levels taken on tang. both curves at bridge				
✓ 146				983.6
T.P.	7.82	1002.52	3.58	994.70

5.1 4.9 6.9 7.9 7.3 7.6 4.6 4.9 4.7 4.7
30 13 9.5 8 9 12.5 17 24 30

3.4 2.8 2.9 7.0 – 6.4 6.4 6.7 3.3 2.4 2.5
27 30 18 12.5 7 4.5 7 12 16 20 25 30

2.3 2.4 5.6 5.0 4.5 4.5 5.0 2.6 2.1 1.7 1.5
30 13 17 7.5 6 7 11.5 16 20 25 30

8.0 7.9 8.1 10.9 11.3 10.7 10.3 10.5 10.8 7.5 7.6
30 19.5 25.5 14 8 6.5 5.5 7 11.5 18 25 30

3.0 3.2 2.8 2.9 5.6 4.1 4.7 5.2 5.0 3.7 3.6
30 25 17.5 11 5.5 4 11 12.5 15.5 25 30

7.7 7.6 7.4 8.3 7.5 8.0 8.4 7.1 7.6
30 16 10 7 7.5 10 14 25 30

11.0 10.8 10.4 10.1 9.4 9.3 10.0 10.6 10.0 10.1
26 19 13 6 5.3 12.5 16.5 20 35 45

4.0 4.3 4.7 4.3 4.5 5.1 4.5 3.8 4.4 3.6
25 14 9.5 4 6 9 14.5 20 25 30

Spike E. root 11" wch. 15' SW of SW 4 bridge
Note: carry ditches away from abut.
10.2 Bridge floor to bottom of abut. stones
9.4 top to bot. abut stones S. End

±25.0 7.2 5.6 5.8 4.7 5.6 6.4 5.5 5.8 6.6
35 15.5 13 11 4.5 6 8.5 13 18.5

		1002.52		
147				986.1
148				988.2
T.P.	6.16	1005.13	3.55	998.97
149				989.5
148 ± 55		30' to break		
149 ± 30		canyon curves S		
T.P.	12.42	1001.39		998.97
149 to		is nearest canyon comes to rd		
150				995.9
+75			± 3.1	
151				997.6
T.P.	3.67	1008.26	6.80	1004.59
152				993.
T.P.	0.34	1004.93		1004.59
153				986.9
T.P.	0.12	992.76	12.29	992.64
154				979.9
155				974.
		Cubt		
T.P.	6.32	989.87	9.21	983.55
156				975.1
BM			8.32	981.55

6.5 5.7 5.4 6.6 6.4 — 6.7 7.1 2.2 2.0 0.8 0.2
30 22 16 13 — 2 4 12.5 18 25 30

1.5 7.3 6.7 6.0 5.5 5.0 4.3 — 5.2 2.3 2.0 1.6 0.6
30 25 19 15 10 7.5 — 9 14 19 25 35

Vert. drop. 14.6 6.4 5.6 — 6.1 2.3 1.6 1.7 0.9 0.0
to creek 25 8 — 8.5 13 16 21 25 35

precipice

± 7.1 6.5 5.6 5.4 6.2 5.5 — 5.8 3.1 3.2 2.5
50' 30 25 19 13 11 — 6 10 18 25 32

5.8 5.1 4.6 4.5 3.8 — 4.3 3.1 3.5 3.1 2.8 3.3
30 22 17.5 12 — 5 9 18.5 22 25 30

5.5 4.6 4.7 5.9 5.0 5.3 — 5.6 3.8 3.5 4.0 3.9
30 18.5 15.5 13 4.5 — 4.5 7.5 10.5 16.5 25 30

6.9 6.8 6.6 8.9 8.4 8.0 — 8.5 5.7 6.0 5.5
27.5 23 16.5 12 8 — 5 8.5 17 25 30

0.6 0.7 0.4 0.9 3.9 3.4 2.8 — 3.5 0.5 1.4 2.0 1.6
30 24 20 15.5 12 9.5 — 5 9.5 14 19 25 30

6.3 6.8 9.0 9.8 9.2 8.7 — 8.9 9.5 7.6 7.3 6.9 6.1 5.6
30 23 18 12.5 10 — 4 6 10 20 23.5 26 30

brush pile 9.15 — 10.6
FL unobtainable — FL
75' fall — 30 32

7.4 7.2 7.3 6.7 7.2 4.8 — 4.2 4.3 4.1 3.5 3.0 3.4
30 25 19 10 3 — 4.5 9.5 12.5 14 25 27 31
E trap

Spike N side tw in Maple 156 ± 18 Lt 35'

		98987			
T.P.	6.28	992.57	3.58	986.29	
157					974.7
+50					977.4
158					974.4
159					975.1
T.P.	5.88	992.08	6.37	986.20	
160					977.1
T.P.	4.45	989.04	7.49	984.59	
161					974.1
T.P.	2.85	987.44		984.59	
162					972.8
BM.			3.64	983.80	
	Culvert				
163					972.5

9.4 9.3 8.3 8.4 8.0 8.2 7.8 7.3 7.3 6.7 6.3
30 19. 14 10 5 3 7 11 19 30
25 25

9.3 9.1 8.7 8.4 7.6 6.2 5.1 5.0 5.7 6.3
35 30 24 21 13 6 20 29 35

8.4 8.6 8.7 8.1 7.6 6.9 6.6
25 17 8 14 22 35
30

10.8 10.6 9.9 8.7 7.6 7.4 7.0 7.7 7.2 6.2 6.7
29 25.5 22 19 10 5 12 17 25 35

5.8 6.5 5.9 6.5 5.4 5.0 4.8 4.5 4.3
22 19.5 10.5 3.5 1.5 11 22 35
27 ¢ trav

6.0 5.5 4.6 5.2 4.9 5.4 4.3 3.4 2.3
30 23 12 10.5 4.5 7 15 30

3.8 3.7 3.1 5.2 5.0 4.7 5.1 2.7 3.0 2.5
26 19 11.5 9 6 7 10.5 15 25 30
29

Spike in 1 foot + 10' Maple 161 ± 95 Lt 30'
8.2 7.9 5.0 7.4
± 22 +L +L

7.0 6.4 5.8 5.3 5.5 5.0 5.4 4.0 4.5 3.8 3.4 2.9
30 19.5 14 10 8 7.5 10 14 17 24 30

		987.44			
T.P.	5.51	989.52	3.43	984.01	
✓ 163+75					975.1
✓ 164					974.6
T.P.	4.68	987.40	6.80	982.72	
	Culvert				
✓ 165					972.6
TP	8.76	991.48		982.72	
+85			4.8 ±		
✓ 166					976.6
	Culvert				
T.P.	4.57	991.45	4.60	986.88	
✓ 167					976.1
T.P.	7.94	994.82		986.88	
✓ 168+01.31					979.6
169			3.0		981.8
169+78			+0.7		984.1
BM.			4.68	990.14	

4.9 4.2 3.7 5.2 4.4 — 4.8 2.7 2.9 2.0
30 18 11.5 8.5 — 6.5 9.5 14 27

4.3 4.2 3.6 4.1 5.8 4.9 — 5.3 2.8 3.0 2.1 1.7
25 19 14.5 11 8.5 — 7 10 14 25 30

Mon 4' N of End culvert

9.3 9.0 5.2 — 6.9
FL inlet F.L. — FL

6.1 5.7 5.2 5.3 5.0 4.8 — 4.9 5.3 4.9 5.1 4.8 5.1
30 16 10.5 8.5 6.5 — 4 7.5 9.5 16 25 30

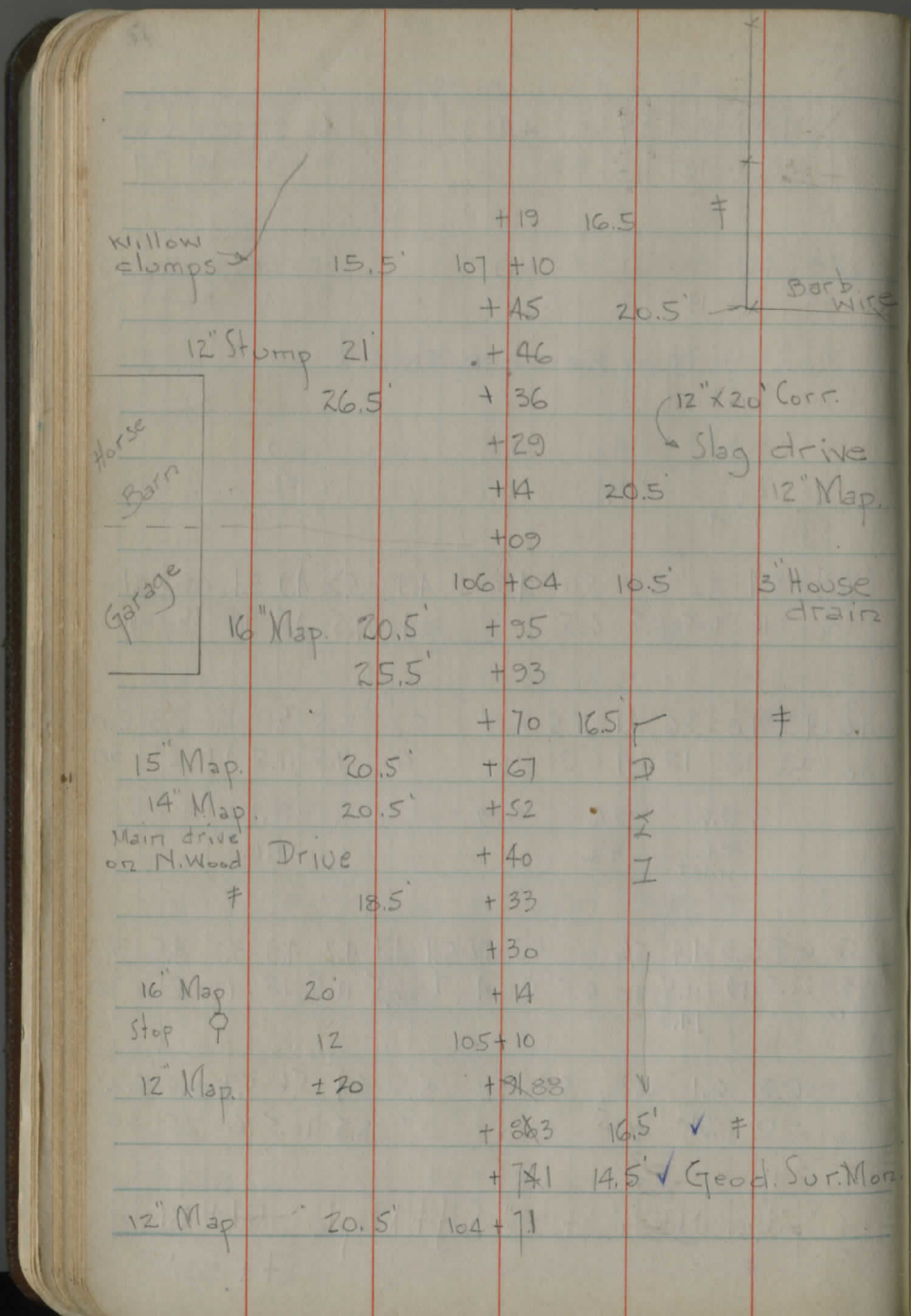
4.6 4.3 4.0 3.6 4.1 5.5 4.9 — 5.2 5.5 3.0 2.6 2.3 2.0
30 23 18 15 11 9 — 4 7.5 11.5 17 25 30

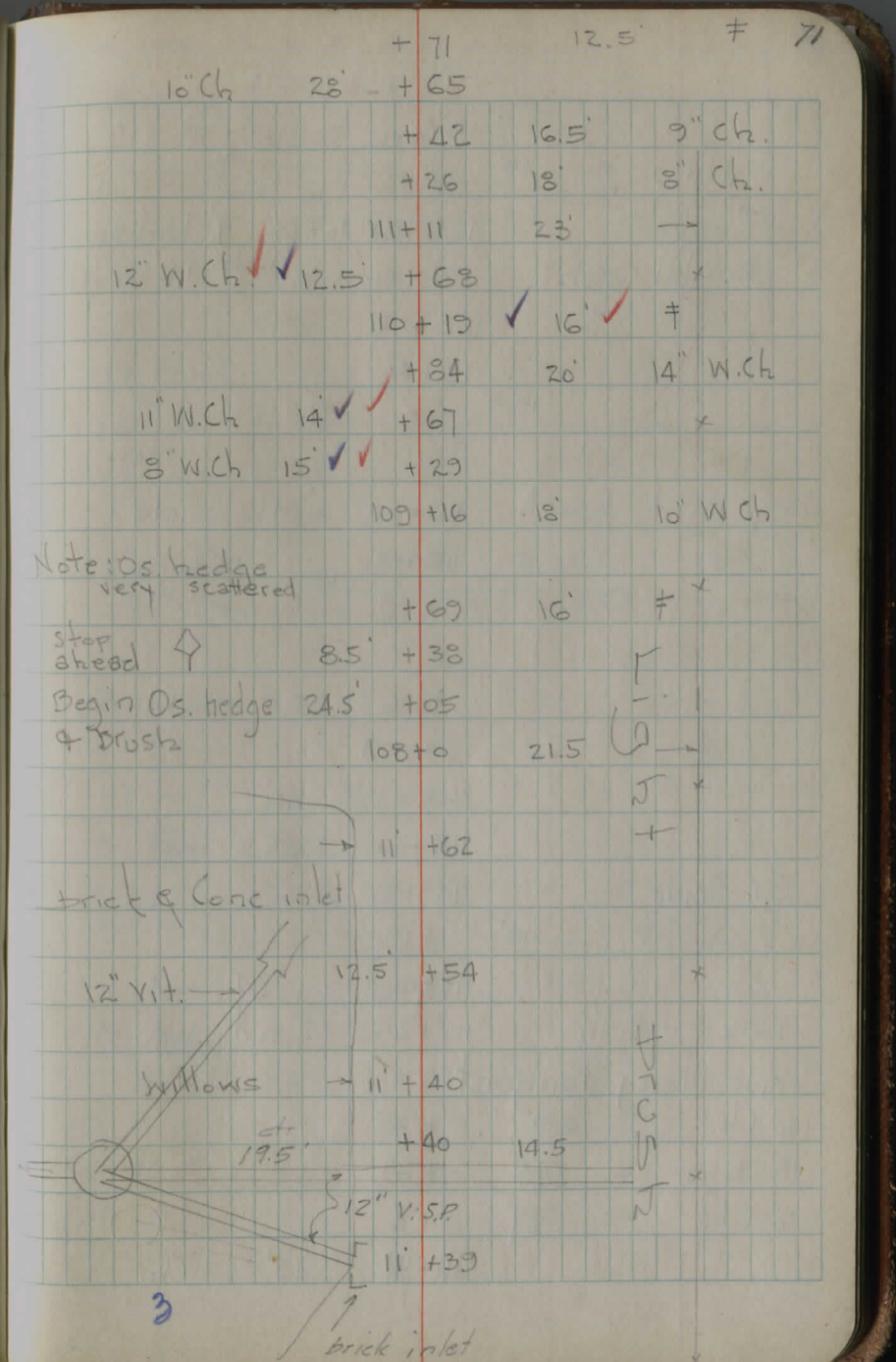
9.6 9.6 5.9 — 8.3
F.L. inlet FL — F.L.

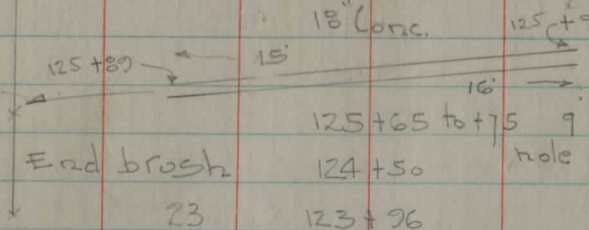
5.0 6.5 6.3 4.4 5.6 – 5.3 5.6 5.7 4.7 4.2 4.3 3.8 3.5 3.3
25.5 22.5 19 11.5 10 6.5 ± 4 7 8.5 11.5 15 19 25 30
30 14.5

6.3 6.1 6.3 5.3 5.2 — 5.5 6.1 5.6 5.7 5.5 5.2
30 24 20.5 9 — 5.5 8.5 10.5 16 25 30

Spike NE root 16" Sgt Maple 51 ± 51
Lt ± 33'


+19 16.5
Willow clumps
15.5'
107 +10
+45 20.5'
Barb Wire
12" Stump 21'
+46
26.5'
+36
12"x20' Corr.
Slag drive
+29
Horse Barn
+14 20.5'
12" Map.
+09
Garage
106 +04 10.5'
3" House drain
16" Map. 20.5'
+95
25.5'
+93
+70 16.5'
15" Map. 20.5'
+67
14" Map. 20.5'
+52
Main drive on N. Wood
Drive
+40
18.5'
+33
+30
16" Map 20'
+14
Stop
12
105+10
12" Map. ±20
+88
+83 16.5'
+71 14.5' Geod. Sur. Mon.
12" Map 20.5'
104+71


+71 12.5'
10" Ch 28'
+65
+42 16.5' 9" Ch.
+26 18' 8" Ch.
111+11 23'
12" W.Ch 12.5'
+68
110+19 16'
+84 20' 14" W.Ch
11" W.Ch 14'
+67
8" W.Ch 15'
+29
109+16 18' 10" W.Ch
Note: Os. hedge very scattered
+69 16'
Stop ahead
8.5'
+38
Begin Os. hedge & Brush
24.5'
+05
108+0 21.5
11' +62
brick & Conc inlet
12" V.I.P.
12.5'
+54
Willows
11' +40
ct 19.5'
+40 14.5
12" V.S.P.
11' +39
3
brick inlet



125+65 to +75 9' bad spring hole tile read

End brush 124+50

23 123+96

122+80

15.5' 17.5' 12" Conc. New

Beg. light brush 119+00 both sides

16.5' 116+85 15' 18" Conc New

+36 25.5' 30" Rep

+21

116+0 26'

115+0 23.5'

Gr. Drive 114+20

℄ 19' +19

113+0 24'

End brush 112+20 End brush

Drive along tangent

10" Ch. 29' +85

18" Elm 24.5' +83

10" Ch. 29' +76

111+74 15' 8" Ch.

10" pop. ✓ 11' ✓ +77

10" pop. ✓ 10' ✓ +71

℄ 14.5' +69

9" V.S.P. +64 8" C.I.P.

13' 9'

Replace with 12"

8" Elm 12.5 +57

36" Pop. ✓ 9' +55

10" Elm 13.5' +51

9" Ash ✓ 10.5 ✓ +49

Begin brush +42 17.5' 10" Elm

+40 21 8" Elm

+26 20' 16" Elm

135+09 23.5' 10" Elm

+50 Begin brush

+41 30' 14" W.Ch

+36 26' 10" Ash

℄ 28' 134+20

CEI Guy 19.5' 134+20

130+53

17' 19' 12" Conc. (New)

20' 128+68

20' +89

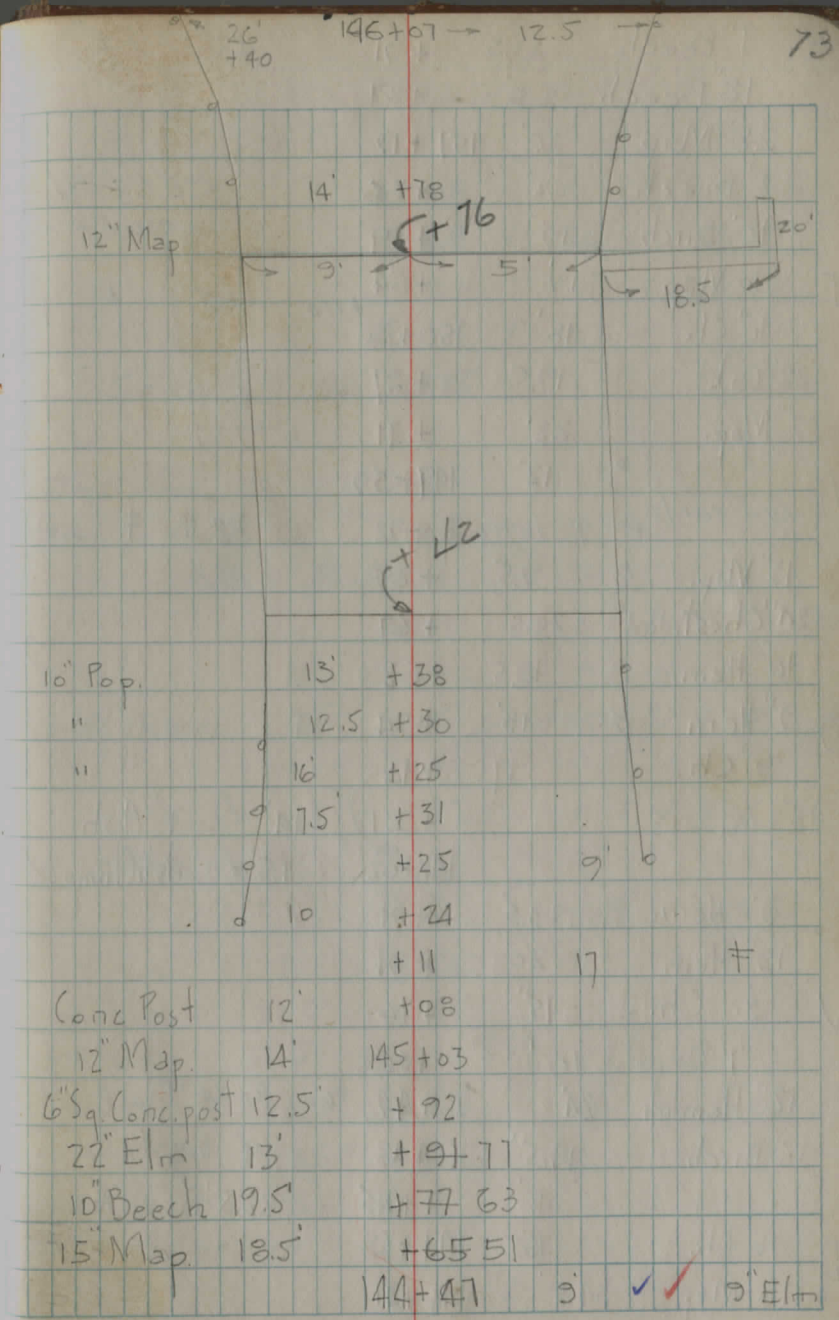
Gr. Drive +50

12" Corr.

21' 126+32

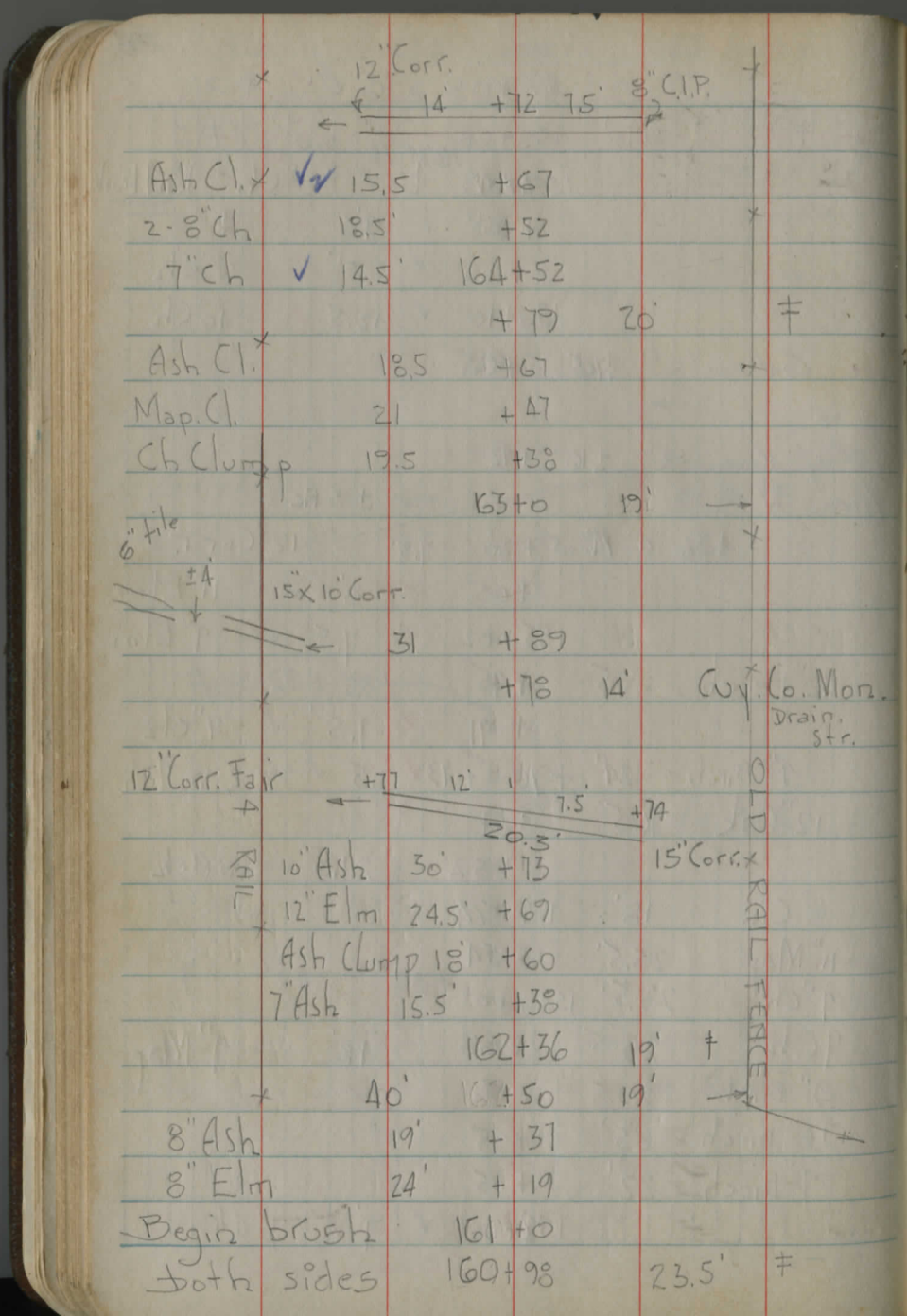
Topo of taken xang

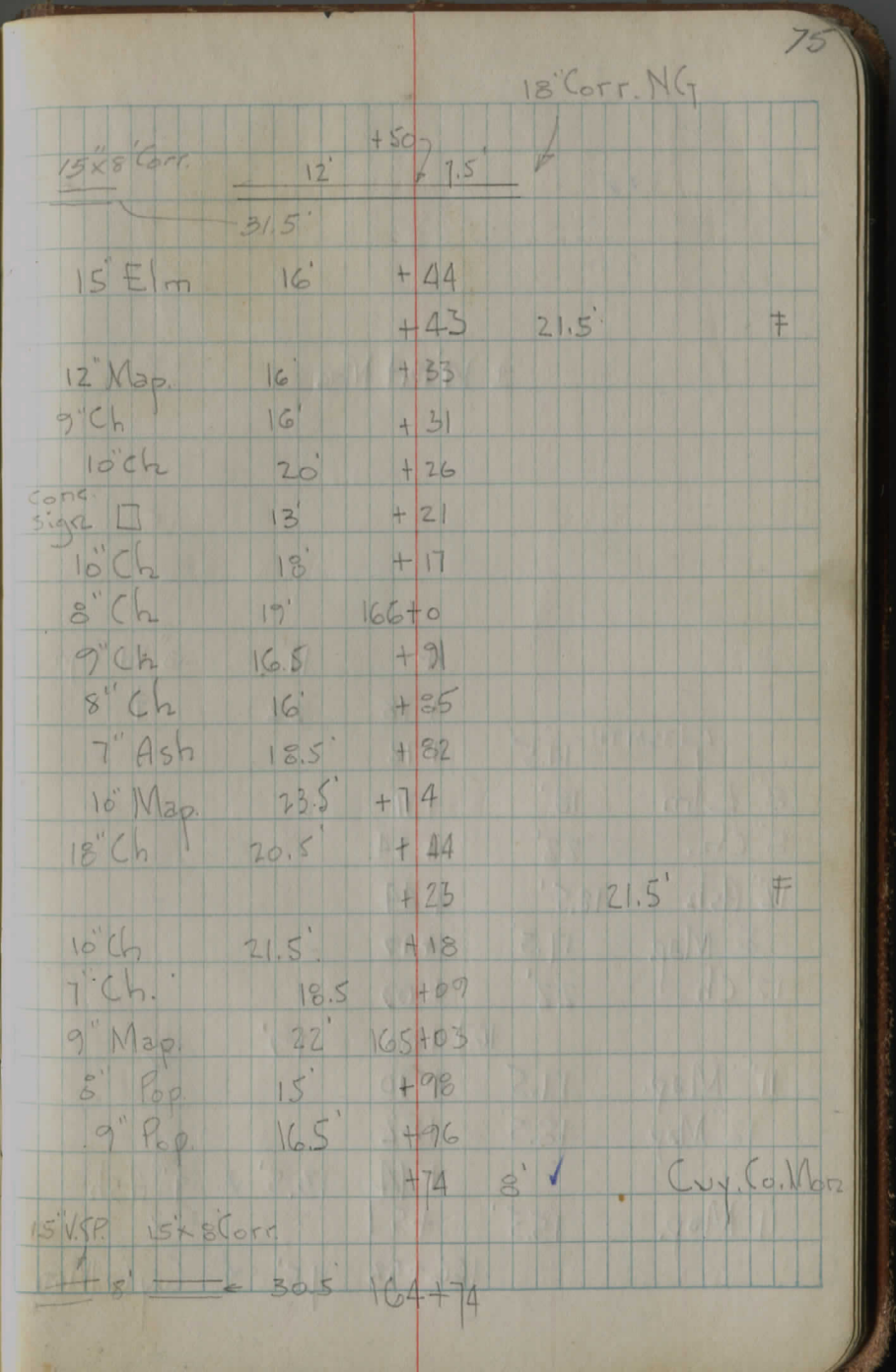
‡	17.5'	+70		
		+28	12'	one Plane bg.
		143+14	18'	Elm (lomp
		+98	17.5'	10" Ash
		+74	14'	8" Ash.
		+10	18'	‡
		142+03	20'	9" Map.
Endbrush		+87		
8" Ap	8.5'	+87		
10" Ch.	13'	141+14		
‡	16.5'	140+50		
		+83	17.5'	8" Elm.
10" Ap.	14.5'	+58		
		+46	22'	8" Ash
8" Map.	10'	+28		
		139+27	21'	12" Ash
‡	16'	+91		
		+97	22'	7" Bass
		+81 ?	21'	8" Bass
		+35	13'	8" Ch.
12" Elm	10.5'	138+02		
8" Elm	10'	+92		
‡	15.5'	+32		
8" Elm	13.5'	+13		
		137+0	25'	W ctr. old rail fence
		135+30	12'	12" Elm



9" Beech 23.5 +91 43' ≠
18" Beech 25' +27
28" Map 26' 151 +19
8" Beech 22' +66 CE1 & Tel comb'd
10" Birch 19' +59
I 16" Map 19' +54 +40 43' ≠ I'
10" Ch 18' 150+30
28" Oak 19.5 +87
9" Map 22' +71
12' 149+59
M Gd rail Z 9' 149+0 +92 32.5 ≠ M
13" Map 9.5 +89
24" Chest. dead 20.5 +67
10" Hem 18.5 +62
9" Hem 13' +54
9" Ch 17' +12
+21 14' 7" Ash
148+02 15' Ash (lump)
9" Hem. 23.5' +91
12" Hem 20' +91
20" Ch. 15' +72
Bone 10' +66
12" Hemlock 24' +49 +60 Horse trail
16" Birch 19.5' +48 9' brush
+45 22.5' ≠
10" Ch. 16' 147+38
18" Map 34.5' 146+41

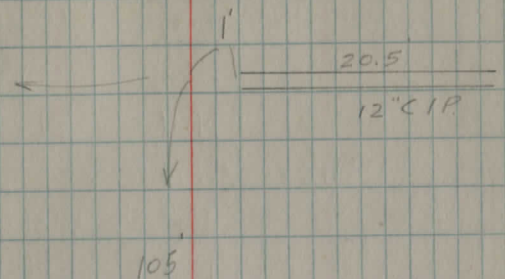
160+05 6'
≠ 20.5' 159+08 157+76 20' ≠
157+48 E Ch Find brush
+28 26' ≠
+23 6.5' 8" Ch
156+10 12.5' 10" Ch
Gd rail Z 9' 14 +75
Step down from G.R. +16 +42 ±3 Ac
+36 d 12.5 +20 7.5' 12" Corr.
+05 8' 11" Elm
155+02 9.5' 9" Elm
12" Beech 25 +95 +85 32.5 ≠
+91 7.5' 9" Ch
9" Birch 24' +70 +73 7.5' 2-10" Ash
12" Oak 16.5 +54
+52 21.5' 10" Ash
8" Ch. 18' 154+24
11" Map 25.5' +54
9" Ch 23.5' 153+00 +35 38' ≠
Ch. 21' +68 18' 9" Map
9" Birch 23.5 +36
10" Birch 25 +35
9" Birch 22' +05
152+08 7' 9" Ch


12" Corr.
14'
+72 75'
8" C.I.P.
Ash Cl. ✓✓ 15.5 +67
2-8" Ch 18.5' +52
7" Ch ✓ 14.5' 164+52
+79 20'
Ash Cl. 18.5 +67
Map. Cl. 21 +47
Ch Clump 19.5 +38
163+0 19'
6" Fill
±4'
15" x 10' Corr.
31 +89
+78 14'
Cuy. Co. Mon.
drain. str.
12" Corr. Fair
+77 12'
7.5'
+74
20.3'
OLD RAIL FENCE
15" Corr.
10" Ash 30' +73
12" Elm 24.5' +69
Ash Clump 18' +60
7" Ash 15.5' +38
162+36 19'
40' +50 19'
8" Ash 19' +37
8" Elm 24' +19
Begin brush 161+0
both sides 160+98 23.5'


18" Corr. NG
+50
15" x 8' Corr.
12' 7.5'
31.5'
15" Elm 16' +44
+43 21.5'
12" Map. 16' +33
9" Ch 16' +31
10" Ch 20' +26
Conc. Sign ☐ 13' +21
10" Ch 18' +17
8" Ch 19' 166+0
9" Ch 16.5 +91
8" Ch 16' +85
7" Ash 18.5' +82
16" Map. 23.5' +74
18" Ch 20.5' +44
+23 21.5'
10" Ch 21.5' +18
7" Ch. 18.5 +09
9" Map. 22' 165+03
8' Pop 15' +98
9" Pop 16.5' +96
+74 8' ✓ Cuy. Co. Mon
15" V.S.P. 15" x 8" Corr.
8' 30.5' 164+74

± 1A Bit Mac

		+	14	6" Rd Sign post
		+ 78	22	‡
	35 MPH 14.5	+ 72		
8" Elm	18'	+ 71		
8" Ch.	22'	+ 54		
12" Ash	18.5'	+ 44		
8" Map.	17.5'	+ 19		
12" Ch	22'	+ 09		
		167 + 00	19'	→
11" Map.	17.5	+ 90		
12" Map	18.5'	+ 82		
		+ 74	13.5' ✓	9" Ash
11" Map.	15.5'	+ 57		
		166 + 53	9.5' ✓	Cuy Co Mon



3705.76

Rec
3706.20

N&V 18" Beech Points at Co. LINE

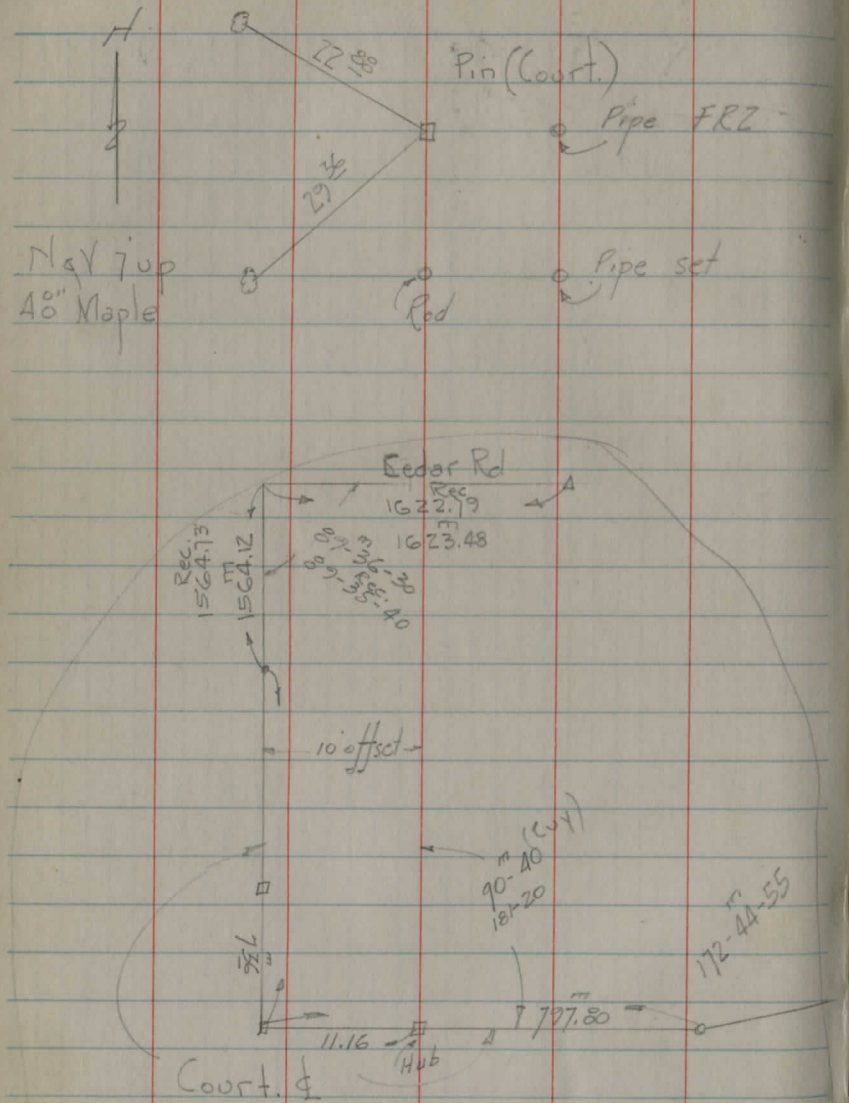


TABLE FOR SLOPE STAKES

Bottom of ditch = base elevation

Approx. existing grade - 1.33' = bottom ditch

Cuts		Fills	Cuts		Fills
	0.1 -	18.3	22.6	+ 2.4 -	25.2
	0.2 -	-.6	.75	.5	-.5
	0.3 -	-.9	.9	.6	.8
	04 -	19.2	23.05	.7	26.1
19.75	+ 0.5 -	-.5	.2	.8	.4
-.9	+ 0.6 -	-.8	.35	.9	.7
20.05	+ 0.7 -	20.1	23.5	3.0	27.0
-.2	+ 0.8 -	-.4	.65	.1	.3
-.35	+ 0.9 -	-.7	.8	.2	.6
20.5	+ 1.0 -	21.0	.95	.3	.9
-.65	+ .1 -	-.3	24.1	.4	28.2
-.8	+ .2 -	-.6	.25	3.5	.5
-.95	+ .3 -	-.9	.4	.6	.8
21.1	+ .4 -	22.2	24.55	.7	29.1
-.25	+ 1.5 -	-.5	.7	.8	.4
-.4	+ .6 -	-.8	.85	.9	.7
21.55	+ .7 -	23.1	25.0	4.0	30.0
.7	+ .8 -	-.4	.15	.1	
.85	+ .9 -	-.7	.3	.2	
22.0	+ 2.0 -	24.0	.45	.3	
-.15	+ .1 -	-.3	25.6	.4	
-.3	+ .2 -	-.6	.75	4.5	
-.45	+ .3 -	-.9	.9	.6	

FULLERTOWN ROAD D E & F

Cuts			
26.05	4.7	29.65	7.1
.2	.8	.8	.2
.35	.9	.95	.3
26.5	5.0		
.65	.1		
.8	.2		
.95	.3		
27.1	.4		
.25	5.5		
.4	.6		
27.55	.7		
.7	.8		
.85	.9		
28.0	6.0		
.15	.1		
.3	.2		
.45	.3		
28.6	.4		
.75	6.5		
.9	.6		
29.05	.7		
.20	.8		
.35	.9		
29.5	7.0		

22-10
18-36-30
3-33-30
10-30
14-03-30

Cedar Rd.

CURVE TABLES.

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HOW TO USE CURVE TABLES.

Table I. contains Tangents and Externals to a 1° curve. Tan. and Ext. to any other radius may be found nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table I.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle of Intersection or I. P. = 23° 20′ to the R. at Station 542+72.

Ext. in Tab. I opposite 23° 20′ = 120.87
120.87 ÷ 12 = 10.07. Say a 10° Curve.

Tan. in Tab. I opp. 23° 20′ = 1183.1
1183.1 ÷ 10 = 118.31.

Correction for A. 23° 20′ for a 10° Cur. = 0.16
118.31 + 0.16 = 118.47 = corrected Tangent.

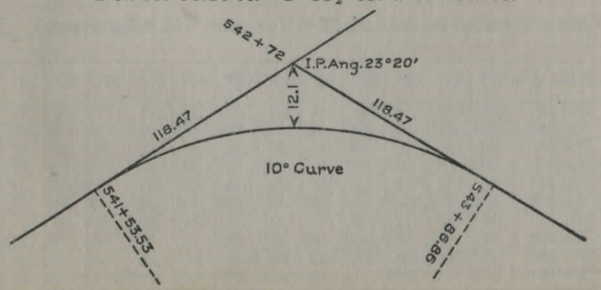
(If corrected Ext. is required find in same way)
Ang. 23° 20′ = 23.33° ÷ 10 = 2.3333 = L. C.

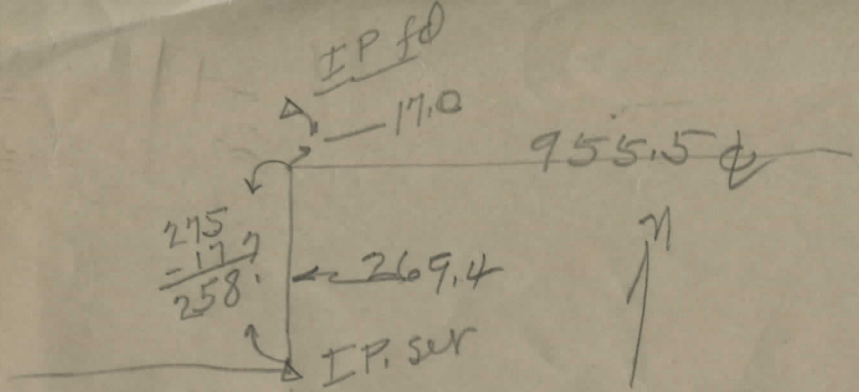
2° 19½′ = def. for sta.	542	I. P. = sta.	542+72
4° 49½′ = " " "	+50	Tan. =	1.18.47
7° 19½′ = " " "	543	B. C. = sta.	541+53.53
9° 49½′ = " " "	+50	L. C. =	2.33.33
11° 40′ = " " "	543+		
	86.86	E. C. = Sta.	543+86 86

100 − 53.53 = 46.47 × 3′ (def. for 1 ft. of 10° Cur.) = 139.41′ =
2° 19½′ = def. for sta. 542.

Def. for 50 ft. = 2° 30′ for a 10° Curve.

Def. for 36.86 ft. = 1° 50½′ for a 10° Curve.




IP fd
17.0
955.5 ℄
275
-17
258.
269.4
N
IP. set

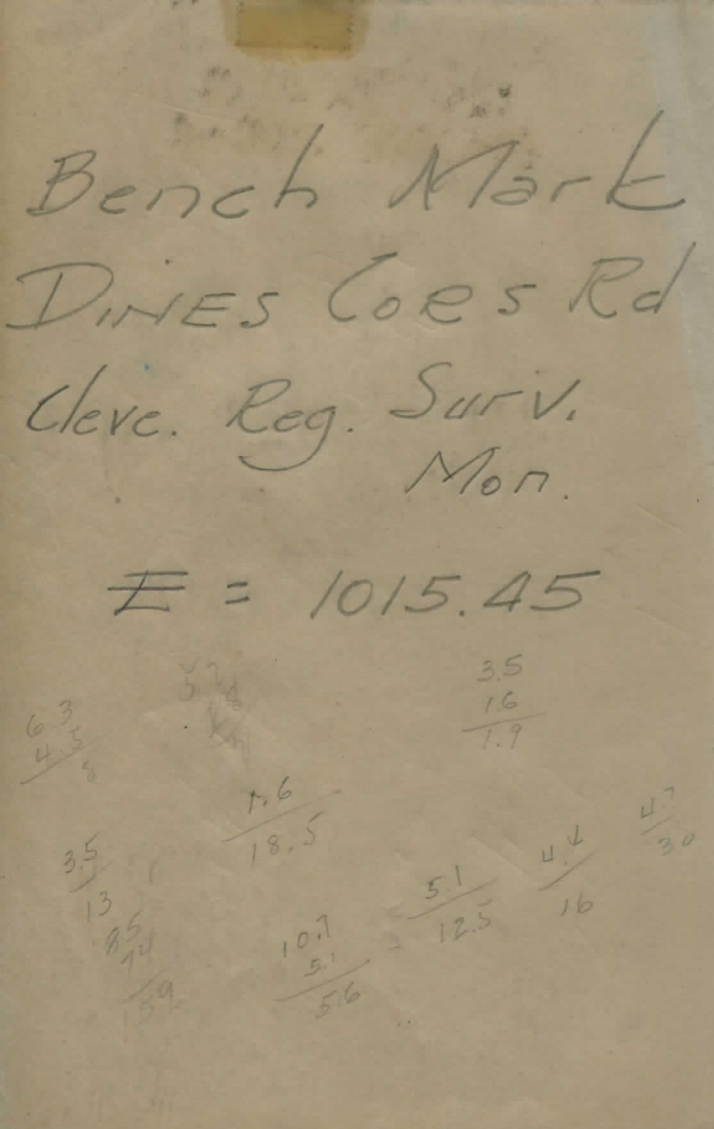
Bench Mark

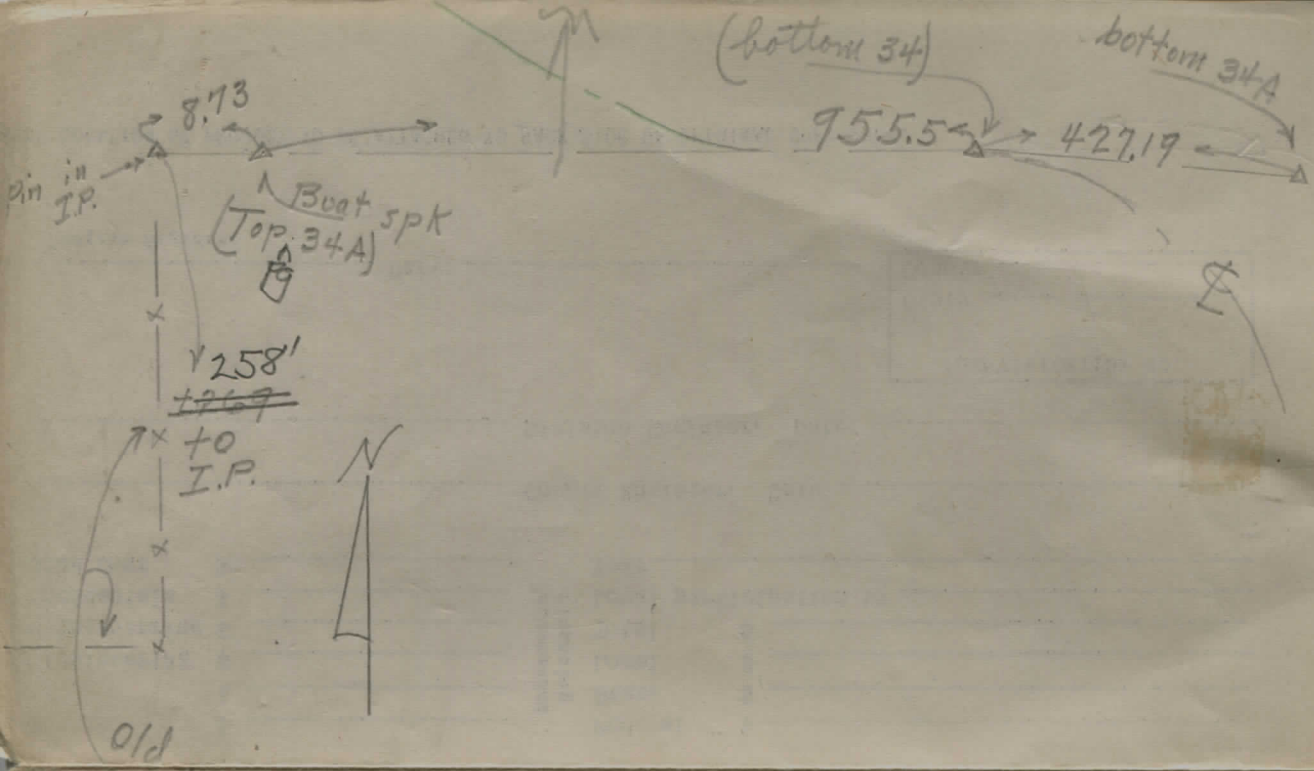
Dines Coes Rd

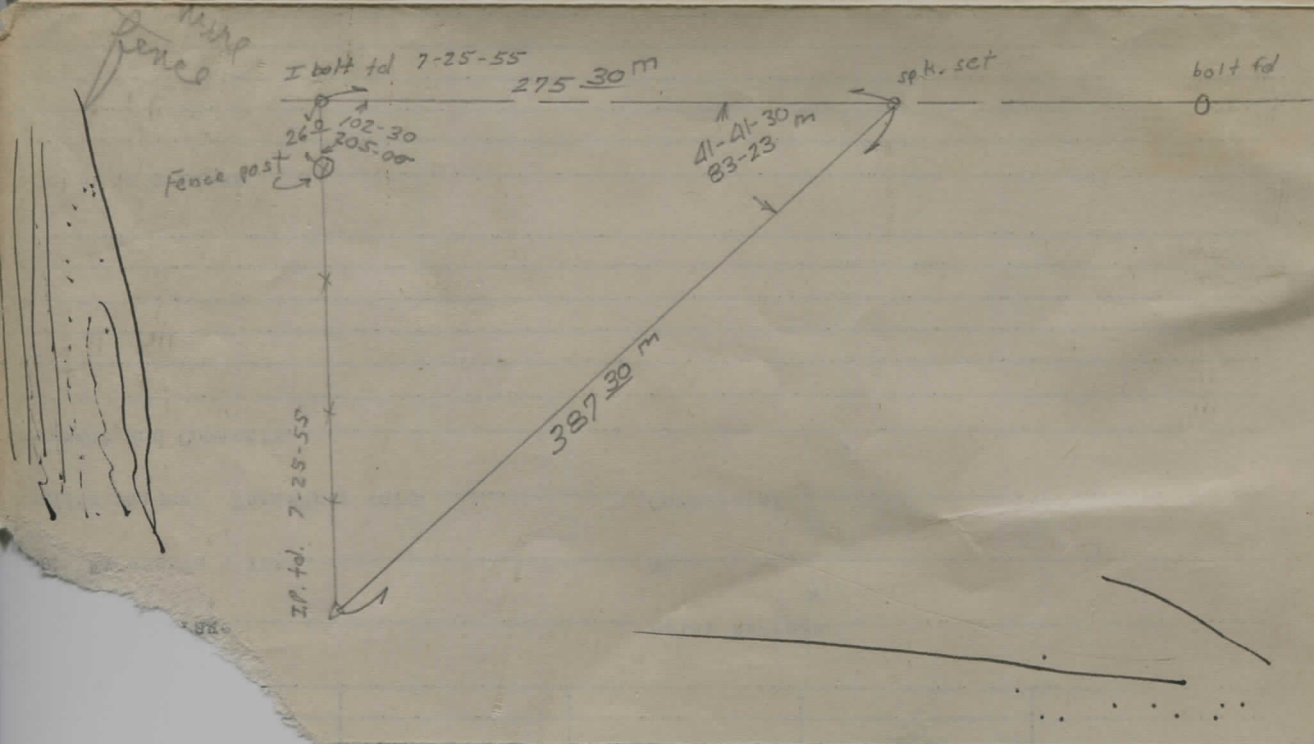
Cleve. Reg. Surv.

Mon.

E = 1015.45




(bottom 34)
bottom 34A
955.5
427.19
8.73
pin in I.P.
Boat spk
(Top. 34A)
258'
+0
I.P.
N
℄
Old
fence


I bolt fd 7-25-55
275.30 m
spk. set
bolt fd
0
26-0
102-30
205-00
Fence post
41-41-30 m
83-23
387.30 m
I.P. fd. 7-25-55

Right Triangle — Oblique Triangles

Solution of Right Triangles

For Angle A. $\sin = \frac{a}{c}$, $\cos = \frac{b}{c}$, $\tan = \frac{a}{b}$, $\cot = \frac{b}{a}$, $\sec = \frac{c}{b}$, $\operatorname{cosec} = \frac{c}{a}$

Given	Required	
a, b	A, B, c	$\tan A = \frac{a}{b} = \cot B, c = \sqrt{a^2 + b^2} = a\sqrt{1 + \frac{b^2}{a^2}}$
a, c	A, B, b	$\sin A = \frac{a}{c} = \cos B, b = \sqrt{(c+a)(c-a)} = c\sqrt{1 - \frac{a^2}{c^2}}$
A, a	B, b, c	$B = 90° - A, b = a \cot A, c = \frac{a}{\sin A}$
A, b	B, a, c	$B = 90° - A, a = b \tan A, c = \frac{b}{\cos A}$
A, c	B, a, b	$B = 90° - A, a = c \sin A, b = c \cos A,$

Solution of Oblique Triangles

Given	Required	
A, B, a	b, c, C	$b = \frac{a \sin B}{\sin A}, C = 180° - (A + B), c = \frac{a \sin C}{\sin A}$
A, a, b	B, c, C	$\sin B = \frac{b \sin A}{a}, C = 180° - (A + B), c = \frac{a \sin C}{\sin A}$
a, b, C	A, B, c	$A + B = 180° - C, \tan \frac{1}{2}(A - B) = \frac{(a-b)\tan \frac{1}{2}(A+B)}{a+b}, c = \frac{a \sin C}{\sin A}$
a, b, c	A, B, C	$s = \frac{a+b+c}{2}, \sin \frac{1}{2}A = \sqrt{\frac{(s-b)(s-c)}{bc}}, \sin \frac{1}{2}B = \sqrt{\frac{(s-a)(s-c)}{ac}}, C = 180° - (A+B)$
a, b, c	Area	$s = \frac{a+b+c}{2}$, area $= \sqrt{s(s-a)(s-b)(s-c)}$
A, b, c	Area	area $= \frac{bc \sin A}{2}$
A, B, C, a	Area	area $= \frac{a^2 \sin B \sin C}{2 \sin A}$

REDUCTION TO HORIZONTAL

Horizontal distance = Slope distance multiplied by the cosine of the vertical angle. Thus: slope distance = 319.4 ft. Vert. angle = 5° 10′. From Table, Page IX. cos 5° 10′ = .9959. Horizontal distance = 319.4 × .9959 = 318.09 ft. Horizontal distance also = Slope distance minus slope distance times (1 — cosine of vertical angle). With the same figures as in the preceding example, the following result is obtained. Cosine 5° 10′ = .9959. 1 — .9959 = .0041. 319.4 × .0041 = 1.31. 319.4 — 1.31 = 318.09 ft.

When the rise is known, the horizontal distance is approximately:—the slope distance less the square of the rise divided by twice the slope distance. Thus: rise = 14 ft., slope distance = 302.6 ft. Horizontal distance $= 302.6 - \frac{14 \times 14}{2 \times 302.6} = 302.6 - 0.32 = 302.28$ ft.